



# BIOCORROSION NETWORK

## A SUM-UP OF FIELD EXPERIENCES

### TASK 2 CORROSION

- Avesta Sheffield AB, Sweden
- BASF, Germany
- British Steel plc, Swindon Technology centre, UK
- Denmark's Technical University, DTU, Denmark
- EDF, France
- Istituto per la Corrosione Marina, Italy
- Sintef, Norway
- Swedish Corrosion Institute, Sweden
- University of Portsmouth, UK



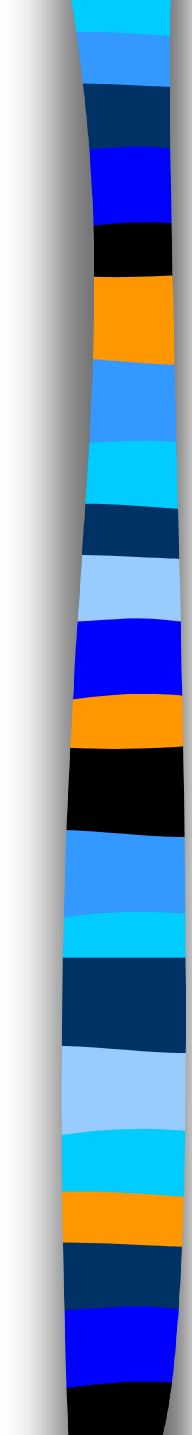
# Introduction

- Carbon Steel in anaerob environments, field studies
- Low alloy steel and carbon steel in anaerob environments, laboratory studies
- Stainless steels anaerob environments, field and laboratory studies
- Stainless steels in aerob environments, field and laboratory studies
- Titanium, Nickel and 70Ni30Cu alloy



# Carbon steel - Low water corrosion

- A statistical comparison between Normal Low Water Corrosion NLWC sites and Accelerated Low Water corrosion (ALWC) sites
- 22 sites in 39 visits where 10 were ALWC sites.



# Accelerated or Normal Low Water corrosion sites

- ALWC site
  - Corrosion rates  $\sim 0.3$  mm/y
  - Local corrosion
  - Corrosion products with poor adherence
- NLWC site
  - Corrosion rates  $\sim 0.1$  mm/y
  - No local corrosion
  - Adherent corrosion products

# Statistical method used

❁ Site ALCW is similar to NLWC

❁ Site ALCW is not similar to NLWC

$ALWC < NLWC$

$ALWC > NLWC$



# Parameter comparison

- General environmental influences: Sunlight rates, mean water/air temperatures and geographical orientations: NLWC = ALWC
- The presence of high number of bacterias (SRB/SOB) did not correlate with low-water corrosion problems.
- No difference in the spatial distribution of bacteria in the layer close to steel surface between the sites.
- Sulphides were qualitatively detected on all sites.



# Corrosion products

The number of culturable bacteria were everywhere lower in the innermost layer in contact with the steel.

<b>PARAMETER</b>	<b>ALWC</b>	<b>NLWC</b>
ORGANIC MATTER	HIGHER	LOWER
ALGAE	HIGHER	LOWER
CHLORIDE	HIGHER	LOWER
HEAVY METALS	LOWER	HIGHER
PH	LOWER UNDERNEATH	HIGHER UNDERNEATH
PHOSPHORUS	LOWER	HIGHER

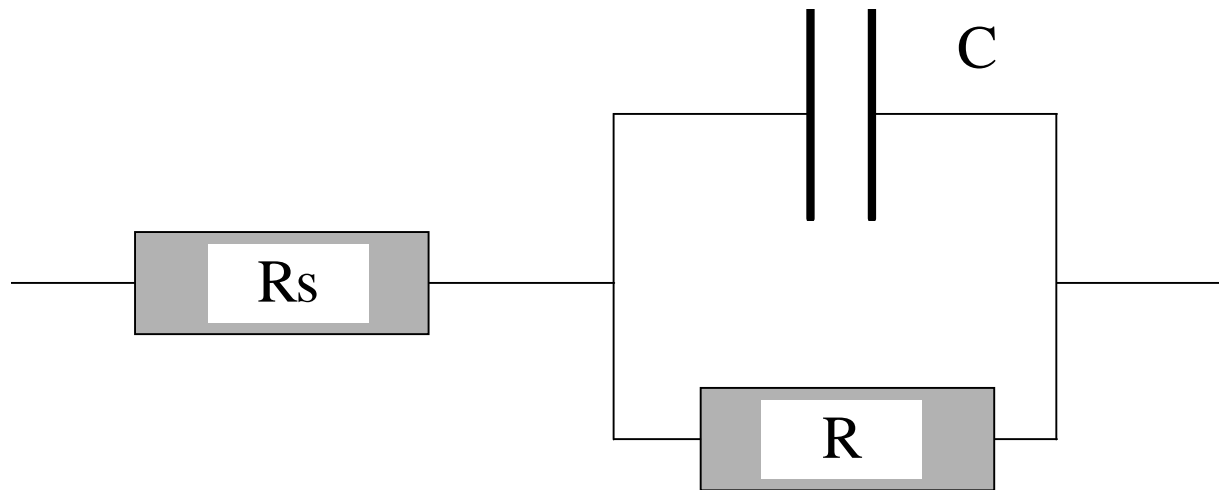
# Statistical significant parameters related to ALWC

	ALWC	NLWC	One tailed t-test
Mean Tidal Range (m)	$3.0 \pm 2.1$	$4.9 \pm 3.0$	ALWC < NLWC P=0.047
- Data from Baltic Sea excluded	$3.5 \pm 2.1$	$5.3 \pm 2.9$	ALWC < NLWC P=0.075
Thickness of Corrosion Products (mm)	$9.7 \pm 6.4$	$6.1 \pm 2.8$	ALWC < NLWC P=0.016
pH underneath Corrosion Products	$6.2 \pm 0.7$	$6.8 \pm 0.7$	ALWC < NLWC P=0.021
Redox Potential of Seawater (mV vs. Ag/AgCl)	$0 \pm 106$	$54 \pm 74$	ALWC < NLWC P=0.05
Presence of Invertebrates	75%	93%	ALWC < NLWC P=0.07
Presence of Algae	90%	67%	ALWC < NLWC P=0.06
Organic Carbon (%)	$2.2 \pm 0.5$	$1.4 \pm 0.5$	ALWC < NLWC P=0.028
Organic Hydrogen (%)	$1.2 \pm 0.2$	$0.8 \pm 0.2$	ALWC < NLWC P=0.041
Organic Nitrogen (%)	$0.36 \pm 0.06$	$0.31 \pm 0.02$	ALWC < NLWC P=0.06
TOC of Seawater ( $\text{mg l}^{-1} \text{O}_2$ )	$14.6 \pm 13.5$	$7.2 \pm 7.9$	ALWC < NLWC P=0.036
MPN <sub>SOB</sub> (Cells $\text{g}^{-1}$ CP dry weight)	$6.5 \cdot 10^5 \pm 2.1 \cdot 10^6$	$3.5 \cdot 10^3 \pm 5.9 \cdot 10^3$	ALWC < NLWC P=0.08



# Carbon steel - anaerob clay, bog - corrosion rates

- Measurements with a probe
- EIS- Electrochemical Impedance Spectroscopy
- Linear Polarisation Resistance measurements



# Corrosion rates

Site, Denmark	Depth in clay	Exposure time	Rate EIS, $\mu\text{m}/\text{y}$	Weight loss, $\mu\text{m}/\text{y}$	Note
Vallensbæk, autumn, 2-12°C autumn	30 cm	6 months	200-400	10	bank, stream Cl- 240ppm
Utterslev, 5-15°C, spring	30 cm	6.5 months	5-10	30	bank, stream
Arresø bog late autumn	30 cm	47 days	init: 200 end: 10	5	marin sediment, stagnant
Kyndby, summer, 15 °C	70 cm	15 days	init: 145	20	SRB active mud, stagnant



# Estimation of corrosion rates with EIS

- The equivalent circuit was not valid for all measurements, but this approach was taken to examine the general change in parameters.
- The risk of erroneous corrosion rate estimation was large especially if porosity was combined with a reactive film



# Field tests in Denmark

- Corrosion rate could not be correctly assessed by EIS if sulphide was present
- DC-polarisation scans were very much effected by hysteresis and did not give a reliable corrosion rate
- Galvanostatic pulse measurements did not give reliable results



## Cont. Field tests in Denmark

- Weight loss measurement was the most reliable technique, but it only gave accumulated corrosion rate.
- All techniques were sensible to the fact that the soil is heterogeneous and that the positioning of probe or weight loss coupons is critical.
- The most active SRB-environment Kyndby was at short time exposure not the most corrosive.

# Low alloy steel and carbon steel - laboratory tests

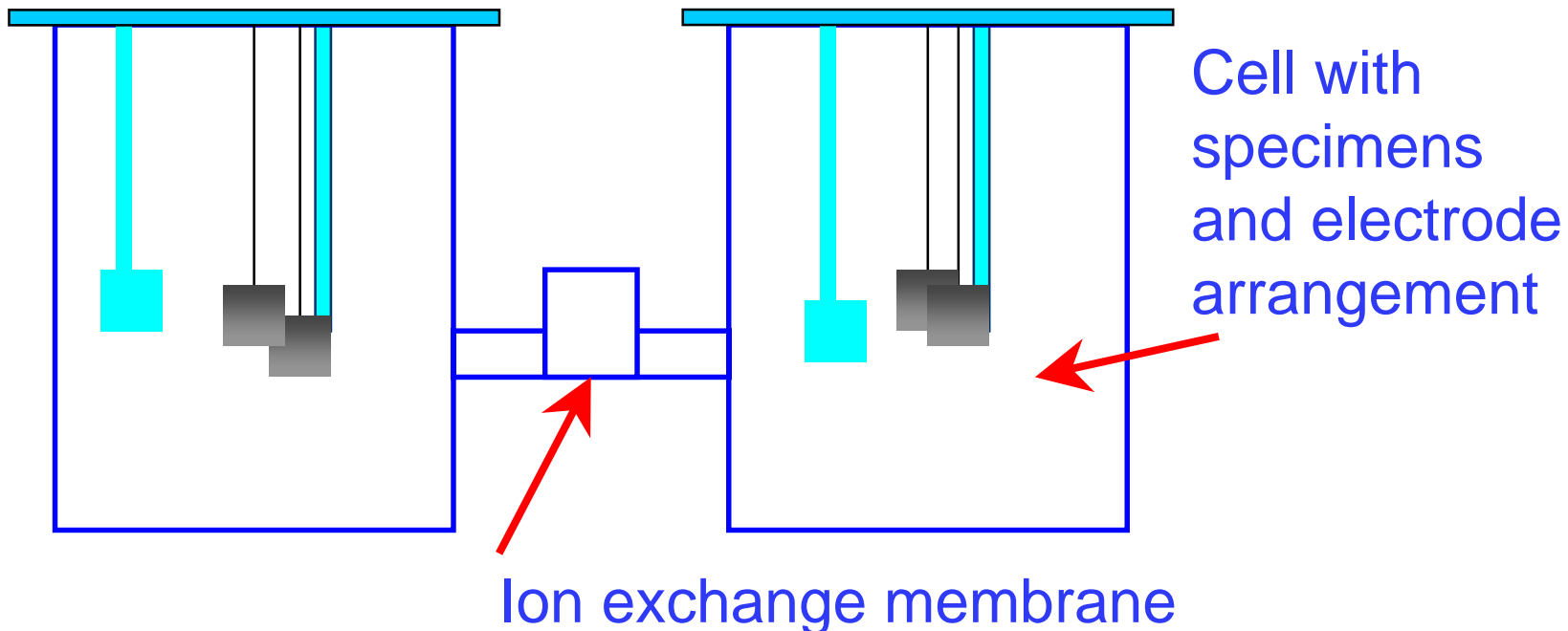
## ■ Material

Nominal composition	C	Si	Mn	P	S	Cr	Mo	Ni	Cu
1%Cr	0.066	0.27	0.95	0.005	0.005	1.02	<0.005	0.04	<0.02
2%Cr	0.081	0.24	0.93	0.006	0.005	1.96	0.006	0.06	<0.02
0.5%Mo	0.069	0.25	0.91	0.006	0.004	0.02	0.490	<0.02	<0.02
0.5%Cu	0.066	0.25	0.97	0.006	0.004	0.03	<0.005	0.04	0.51
1.85%Si 0.25Cr	0.060	1.85	1.04	0.014	0.004	0.25	-	-	-
1.35%Si 0.55%Cr	0.080	1.35	1.00	0.015	0.005	0.56	-	-	-
CrNiCu	0.057	0.43	0.74	0.012	0.005	0.90	-	0.23	0.29
Mild steel	0.110	0.04	0.53	0.012	0.007	0.02	-	0.02	<0.02

# Experimental

- Dual cell arrangement

- Filtered 0.2  $\mu\text{m}$  Portsmouth seawater
- consortia COT, SOB, SRB to one of the cell



# Results - low alloy steel and carbon steel, laboratory test

Steel grade	Corrosion rate (mm/y)	Comments
1% Cr	1.44	Inoculated
	0.04	Uninoculated
2% Cr	1.38	Inoculated
	0.39	Uninoculated, black deposits
0.5% Mo	1.59	Inoculated
	0.13	Uninoculated
0.5% Cu	1.06	Inoculated
	0.13	Uninoculated
1.8%Si, 0.25% Cr	1.40 (2.28)	Inoculated
	0.17 (0.16)	Uninoculated
CrCuNi	0.50 (1.02)	Inoculated
	0.13 (0.16)	Uninoculated
Mild steel	1.64	Inoculated
	0.08	Uninoculated





# Low alloy steel cont.

- Inoculated cell
  - Black deposits, increased corrosion rates
- Uninoculated cell
  - Low corrosion rates



# Biological drum reactor - laboratory tests

- Carbon steel AISI-SAE 1008
  - Three experiments, duration time: 70-120 days
  - 40 coupons,  $\varnothing 10$  mm in a 120 dm<sup>3</sup> drum reactor containing artificial seawater (ASTM D1141-80) inoculated with SRB
  - Anaerob environment by Nitrogen gas purging
  - Inoculation with crude oil terminal SRB
  - Flow by rotation: 60 rpm
  - Temperature: 20-22°C
  - Chloride content: 17.7 ppm



# Biological drum reactor, results

- General corrosion with a tendency to locality
- Initial corrosion rates determined with LPR and DC:  $10 \mu\text{m}/\text{y}$  that increased to  $2 \text{ mm}/\text{y}$  after film formations
- Corrosion rates determined with EIS:
  - initial  $10\text{-}100 \mu\text{m}/\text{y}$
  - final  $1\text{-}2.5 \text{ mm}/\text{y}$
- EIS: large capacitance as sulphide concentration increased
- OCP:  $-750 \text{ mV}/\text{SCE}$  that increased after film formation to  $-650 \text{ mV}/\text{SCE}$

# Stainless steels

- Anaerob environment
  - Seawater, clay
  - Wastewater treatment
- Aerob environment
  - Seawater
  - River water
  - Wastewater



# Crevice corrosion resistance in anaerobic seawater

- Material: Stainless steel grades, 1.4404 (316L), 1.4539 (904L), 1,4462 (2205), 1.4547 (254SMO) and 1.4652 (654SMO) with crevice formers of polyethylene
- Environment: Marine anaerobic bacteria SRB from a natural source fed with milk
  - Temperature: 30°C, pH 6.85-7.1
  - Sulphide: 320-500 ppm

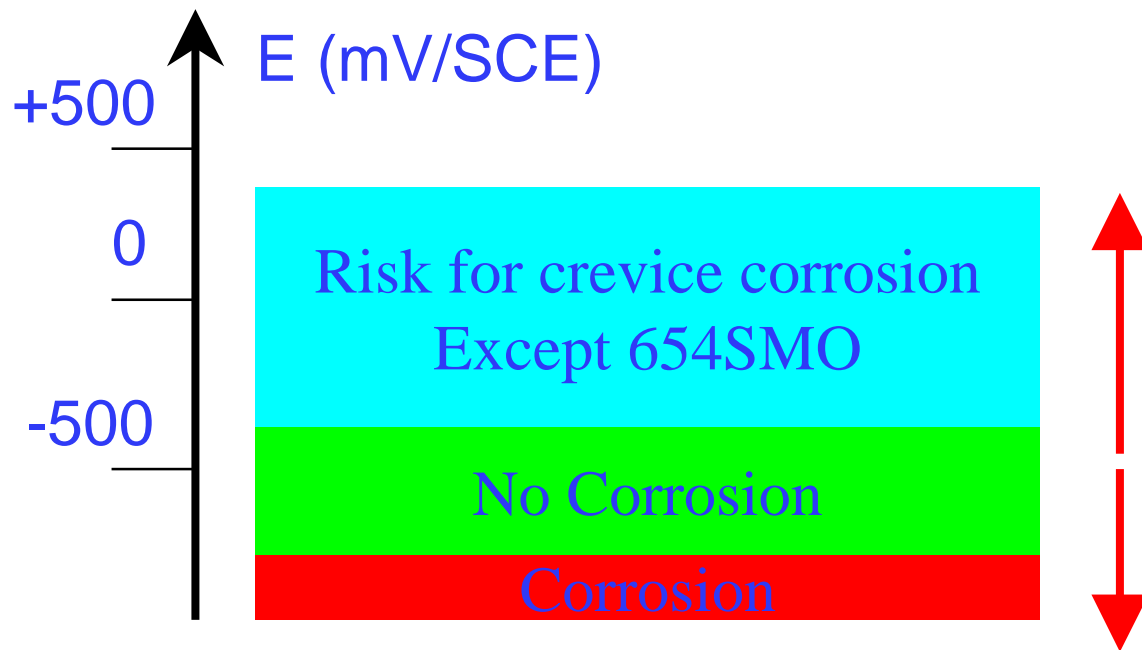


# Stainless steels and anaerob environment - seawater

- Electrochemical measurements: OCP, potentiodynamic polarisation scans (cathodic, anodic)
- Simulation of ennoblement in anaerobic environment corresponding to a coupled situation between anaerobic environment and aerobic environment (2mV/15 min)

# Stainless steels - anaerob seawater, crevice corrosion

- OCP in anaerob environment  $\sim -550$  mV/SCE
- No corrosion in a pure anaerobic environment
- Coupled situation in positive or negative direction can give an increased risk for crevice corrosion





# Stainless Steel - Seawater polluted with sulphide

- 1.4401(316), 1.4462 (2205), 1.4447 (254SMO), 1.4652 (654SMO)
- Crevice samples simulating real flange situations.
- Exposure in a tank (5m<sup>3</sup>) with recirculated seawater (30-40 dm<sup>3</sup>/h) for 95 days.
- Addition of 1000 ppm Na<sub>2</sub>S in the start of the test.





# Results - SS in Seawater polluted with sulphide

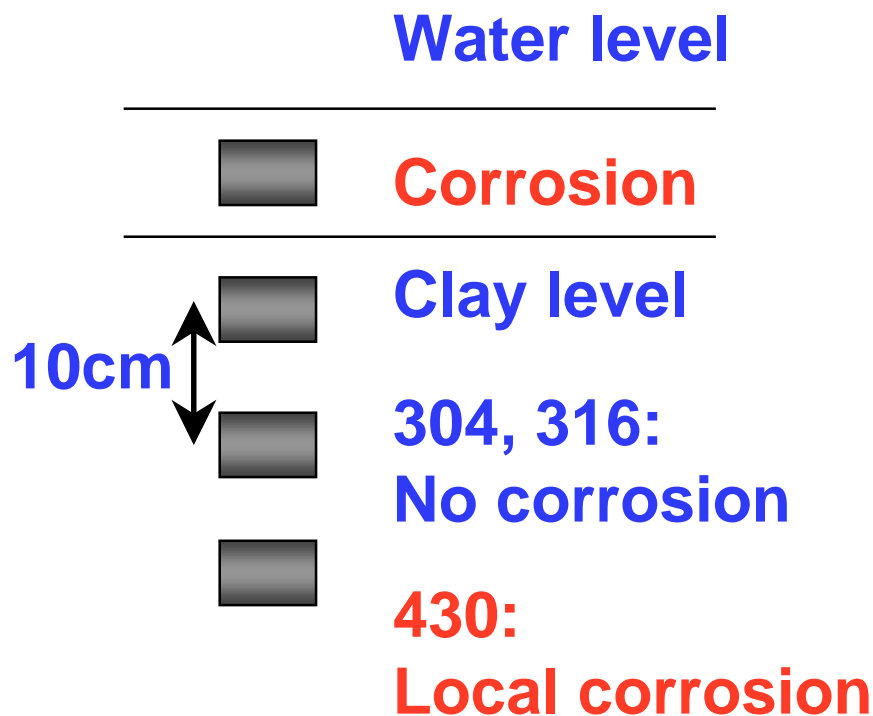
- OCP ~ -515 mV/SCE,
- Redox ~ -500 mV/SCE
- Attacks on 1.4401 (316) at welds and at dark brown spots in the fusion line
- Pitting on 1.4401 (316) above the waterline



# Chlorinated seawater

- 1.4401(316), 1.4462 (2205), 1.4447 (254SMO), 1.4652 (654SMO) and nickel based alloys N06625, N10276
- Crevices simulating real flange situations
- Residual chlorine 7.7-13 ppm (~10 ppm)
- pH 8.0-8.1, Temperature 45°C
- No slime or biofouling after 95 days exposure
- Corrosion on all samples except 654SMO

# Anaerobic clay environment in seawater at Genova harbour



- Stainless steel grades  
1.4013(430) 1.4301(304)  
1.4401(316)
- Exposure 6 months
- pH 7.6
- Sulphur content 2.65-3.15  
mol/dm<sup>3</sup>
- OCP: 304, 316 ~ -500
- OCP: 430 ~ -500 to -600



# Stainless steels in aerob environment

- Seawater - MAST program - Biofilm project, Marine Biofilms on stainless steels, Effects, monitoring and prevention
- Fresh water and industrial system
  - River Rhine
  - Chemical plants
  - Wastewater
  - Nuclear Power Plants

# MAST II

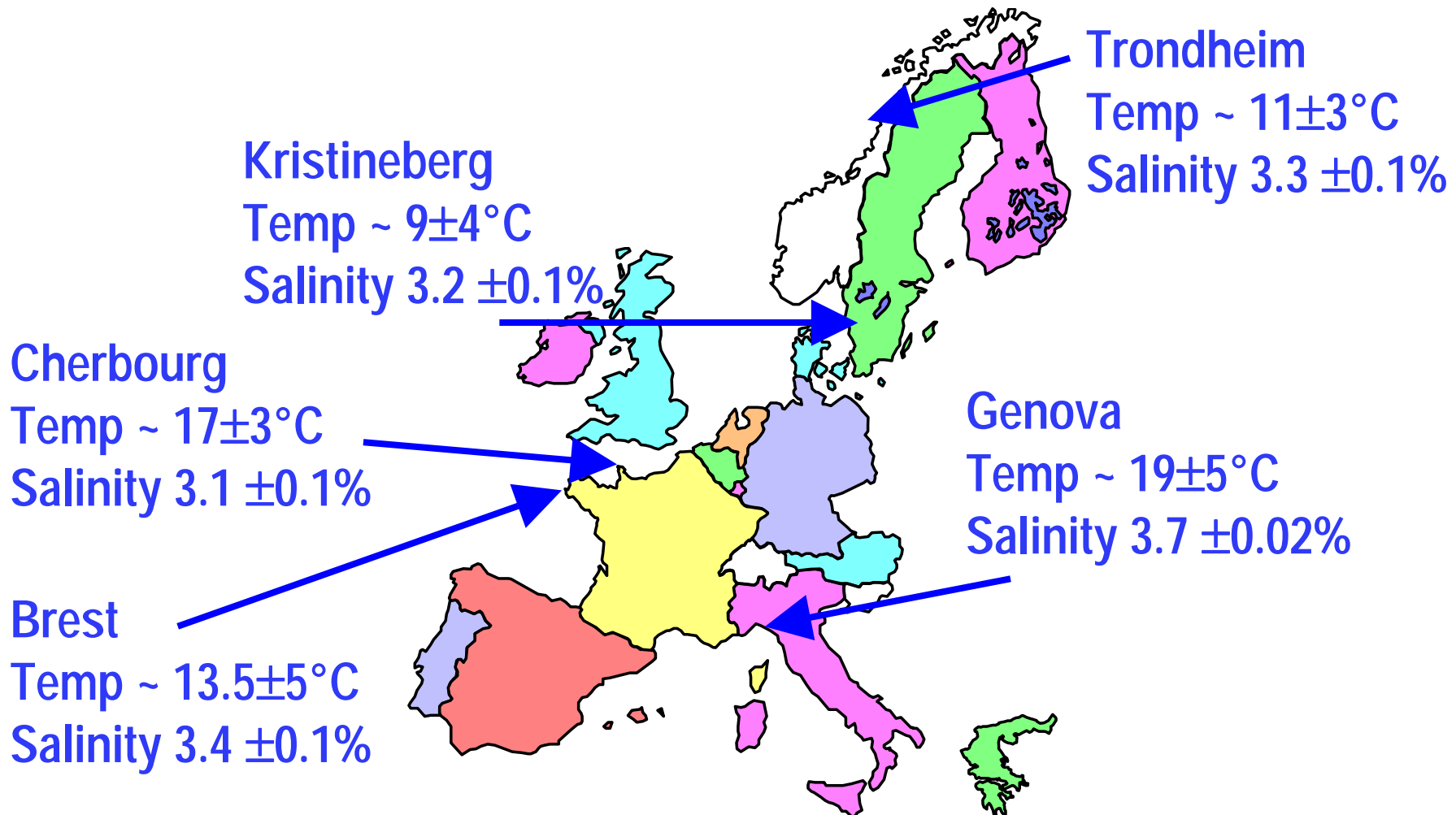
- Exposure in coastal seawaters in Europe with and without crevices (POM)
- Biofilm samples were collected to relate electrochemical effects to biofilm components

Table 1. Stainless steel grades exposed in the MAST II Program.

EN	Trade name	Chemical composition, (% weight)				
		Cr	Ni	Mo	Cu	N
1.4435	316L	17.2	12.6	2.6		
1.4462	2205	22	5.5	3.2		0.17
1.4460	UR47N	24.7	6.6	2.9		0.18
1.4507	UR52N+	25	6.3	3.6	1.5	0.25
1.4410	SAF 2507	24.9	6.9	3.8		0.28
1.4547	254SMO	19.9	17.8	6	0.69	0.2
1.4652	654SMO	24.5	21.8	7.3	0.43	0.48
1.4563	SAN28	26.7	30.3	3.4	0.9	0.07
1.4537	URSB8	24.9	25	4.72	1.4	0.21
1.4529	URB26	20	24.7	6.3	0.8	0.19

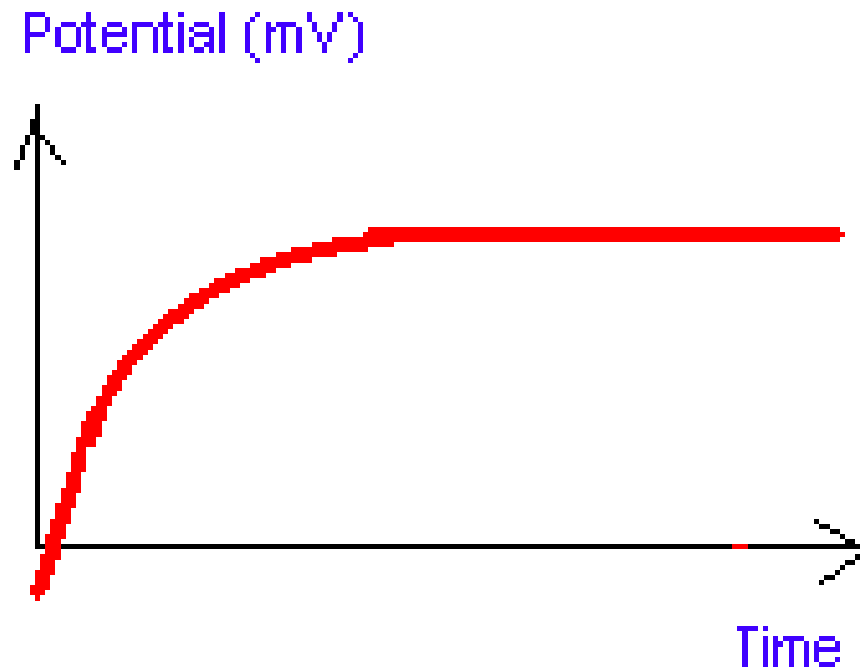
# Geographical locations

- Exposure time : summer 93 - spring 94



# Seawater exposure

- Potential ennoblement and final value at all stations and seasons similar
- Initial OCP varied
- Incubation time varied with season





# Seawater exposure, cont.

## ■ No correlations with ennoblement:

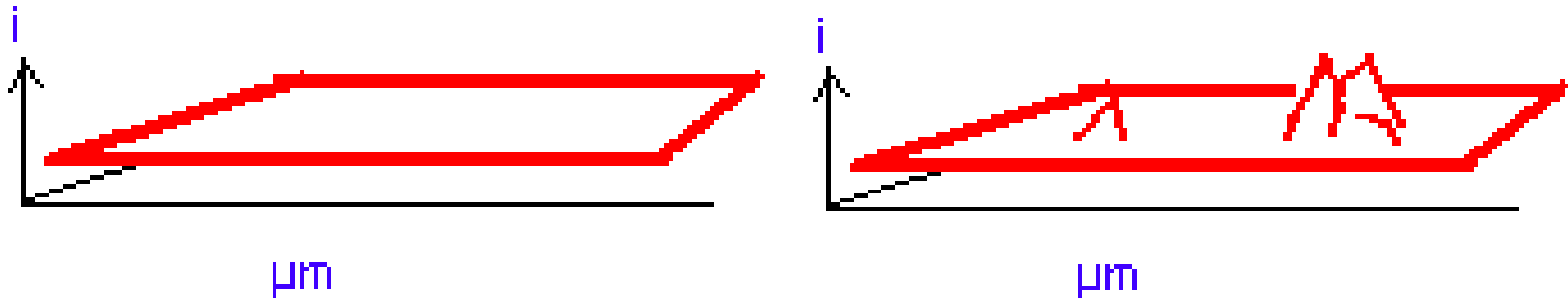
- pH
- geographic location
- stainless steel compositions
- chlorophyll a
- salinity
- ash
- organic matter contents, biomass

## ■ Related to ennoblement:

- Temperature
  - 20°C rapid increase of potential
  - 30°C rapid increase of potential
  - 40°C no ennoblement
- EPS content (satisfactory correlation)



# Biofilm growth and cathodic current evolution - SVET



- After one day of exposure, the oxygen reduction current was uniformly distributed over the whole stainless steel surface (1.4410, SAF2507)
- 50 days exposure in Baltic seawater in the laboratory showed preferential sites for a fast oxygen reduction
- By adding an enzymatic inhibitor the active sites were deactivated



# Corrosion after exposure

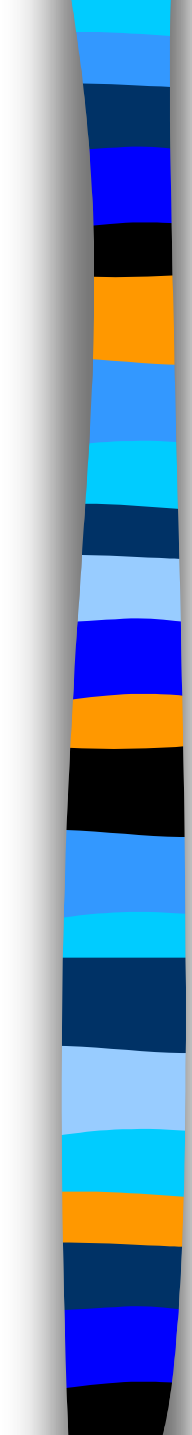
- Crevice corrosion was found on 316 L exposed in Genoa, Italy and Trondheim, Norway
- The more alloyed steel grades either austenitic or duplex grades appeared to be resistant to crevice corrosion after 250 days (6000 hours) at all stations
- Depassivation (discolouration) appeared but there was no weight loss



# MAST II - Experiences on real industrial components

- Cases of corrosion failures that occurred in seawater systems at installations in the North Sea
  - Crevice corrosion in flanges
  - Treads with critical geometry for initiation
  - Improper surface treatment
  - Chlorinated systems on higher alloyed 6Mo Stainless Steel

# Industrial systems

- 
- Chemical plant using cooling water from River Rhine, 1.4401
    - Flow 1.5-2 m/s
    - Cl<sup>-</sup> ~ 50-200 ppm,
    - Temperature 30-35°C
    - Pitting corrosion - pinhole leaks on welds
    - No corrosion on base material
    - Unpickled welds remaining heat tints
  - Tubular heat exchanger
    - leaked after 5 years service 1.4462(2205) welded with (X2CrNiMoN17-13-5)
    - Temperature 30-50°C
    - Used for some weeks/year - often stagnant flow conditions dominated
    - River water remained in the tubes

# Wastewater treatment

- Corrosion of SS 1.4404 (316L) pipes in a wastewater treatment plant after modernising with biological nitrification/denitrification unit; pharmaceutical plant
- 19 year corrosion free
- Six months after taking new unit into use:
  - Pitting at welded joints
  - Pitting nearly on nearly all circular welds
  - Pitting on base material but no leaks
  - Pitting and crevice corrosion on flanges and nozzles



# Wastewater treatment, cont.

- Field tests in the final stages in four plants in Sweden for one year on 1.4301 (304), 1.4401 (316), 1.4462 (2205)
- Ennoblement: in two plants and with values close to the same as in seawater in one of the plants
- Corrosion was found on 1.4401(316) in one plant both on welds and base material
- Corrosion on 1.4301 (304) in three of the plants
- No corrosion on 1.4461 (2205)



# Nuclear Power plant

- Fire protection system in a power plant and waste treatment system
- 1.4301 (304) 18-10 welded tubes
- 300-500 ppm chloride
- 100 ppm sulphate, pH 7.5-7.9
- Room temperature
- Leaks on the welds after one year
- Loop test with river water and sterilised water
- Enhanced corrosion in raw water loop
- Biofilm development on unpickled welds

# Titanium, Nickel and 70Ni70Cu alloy - laboratory study

- Immersion in a tank of 100 dm<sup>3</sup> of natural seawater changed with renewal 100dm<sup>3</sup>/h and in unchanged sterilised seawater, temperature: 25°C
- Ti: increase in the free corrosion potentials  
~250mV/SCE in natural water
- Ni: Similar free corrosion potentials in natural and steril water but corrosion was found by weight loss
- 30Ni70Cu alloy: Similar free corrosion potentials in both environment but corrosion was found by weight loss



# Conclusions



Discussion