Appendix 1

List of participants

Minutes of EFC WP15 Corrosion in the Refinery Industry 24 March 2022

NAME	SURNAME	COMPANY	COUNTRY		
Arzuffi	Mirko	Amec Foster Wheeler	ITALY		
Baak	Michael	Borealis Polyolefine GmbH	AUSTRIA		
Ciocca	Federico	Donegani Anticorrosione	ITALY		
Claesen	Chris J	Nalco Champion	BELGIUM		
Comas	José	Total Refining & Chemicals	FRANCE		
Corradini	Raffaele	Techint Engineering Construction	ITALY		
Daly	Simon	Hempel UK Ltd	UK		
De Landtsheer	Gino	Borealis	BELGIUM		
de Marco	Marco	Istituto Italiano della Saldatura	ITALY		
Dupoiron	François	IDEMAC	FRANCE		
Farina	Carlo	CEFIT Corrosion Consultant	ITALY		
Goti	Raphael	Total Refining & Chemicals	FRANCE		
Gregoire	Vincent	Equinor	NORWAY		
Groysman	Alec	Israeli Corrosion Forum	ISRAEL		
Hairer	Florian	Linde, Engineering Division	GERMANY		
Hamed	Noreldaim	SENDAN INTERNATIONAL COMPANY	SAUDI ARABIA		
Hermse	Chretien	Shell Moerdijk	NETHERLANDS		
Höwing	Jonas	Sandvik	SWESEN		
Jayabalan	Thangavelu	INERIS	FRANCE		
Kittel	Jean	IFP Energies nouvelles	FRANCE		
Koller	Swen	Holborn Europa Raffinerie GMBH	GERMANY		
Kroth	Matthias	OMV Deutschland Operations GmbH & Co. KG	GERMANY		
Kus	Slawomir	Honeywell	UK		
Le Manchet	Sandra	Arcelor Mittal	FRANCE		
Leone	Antonino	Eni	ITALY		
Lobaton Fuentes	Militza	Borealis Chimie SAS	FRANCE		
Low	Philip	Zerust Oil andGas	SPAIN		
Maffert	Joerg	Dillinger Huttenwerke	GERMANY		
Magel	Chris	PPG Protective & Marine Coatings	BELGIUM		
Makhoul	Roger	Spraying Systems MENA Co	UNITED ARAB EMIRATES		
Matthews	Dale	Zerust Oil andGas	SPAIN		
Miyashita	Junki	MODEC, Inc	BRAZIL		
Monnot	Martin	Industeel	FRANCE		
Narjoz	Cyril	IGS EUROPE	FRANCE		
Norling	Rikard	RISE	SWEDEN		
Onodera	Yoichi	Mitsui & Co Ltd	JAPAN		
Pålsson	Namurata	RISE	SWEDEN		
Pojtanabuntoeng	Thunyaluk	Curtin University	AUSTRALIA		
Rehberg	Thomas	KAEFER Isoliertechnik GmbH & Co. KG	GERMANY		
Renaud	Lionel	Total raffinage Chimie	FRANCE		
Rivero	Andres		NORWAY		
Rodriguez Jorva	Javier	Equinor CEPSA	SPAIN		
° .		IFP Energies nouvelles	FRANCE		
Ropital	François		UK		
Sharma	Prafull	Corrosion RADAR			
Surbled	Antoine	A.S – CORR CONSULT	FRANCE		
Uusitalo	Mikko	Valmet Technologies, Inc.	FINLAND		
Van Dooren	Piet	Borealis	BELGIUM		
van Roij	Johan	Shell Global Solutions International B.V.	NETHERLANDS		
Vanacore	Alessandro	Donegani Anticorrosione	ITALY		
Vlad Voca aluí	Gogulancea	LUKOIL Neftochim Bourgas JSC	ROMANIA		
Vosecký	Martin	Nalco Champion	CZECH REPUBLIC		
Wassink Watt	Casper Clare	Eddyfi Technologies KAEFER Isoliertechnik GmbH & Co. KG	NETHERLANDS GERMANY		
		Stork			
Wijnants	Geert Henk		NETHERLANDS		
Wold	Kjell	Emerson	NORWAY		
Yanes Guardado	Maria Jose	REPSOL	SPAIN		
Yuhei	Suzuki	Nippon Steel Europe GmbH	GERMANY		
Zakeri	Hadi	Petrolneos	UK		
Zhang	Jian-Zhong	SABIC			
Zlatnik	Ivan	MITSUI & Co Deutschland	CZECH REPUBLIC		

Appendix 2

EFC WP15 Activities

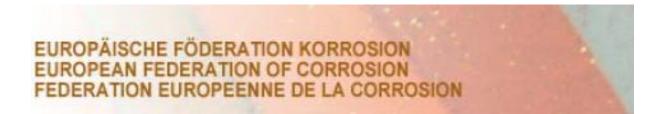
(Francois Ropital)



Welcome to the EFC Working Party Meeting

"Corrosion in Refinery and Petrochemistry" WP15

24 March 2022



EFC WP15 spring meeting 24 March 2022



Stefan passed away on 12th December 2021.

Stefan gave great contributions to our corrosion activities.

Stefan was the initiator and the driving force for the EFC green book on Corrosion Under Insulation.

Stefan will always stay in our minds.









EFC Working Party 15 « Corrosion in Refinery and Petrochemistry » Activities

Chairman: Francois Ropital Deputy Chairman: Johan Van Roij <u>Information Exchange - Forum for Technology</u> Sharing of refinery materials /corrosion experiences by operating company

representatives (ie corrosion atlas).

Sharing materials/ corrosion/ protection/ monitoring information by providers

<u>Eurocorr Conferences</u>: organization of refinery session and joint session with other WPs (2022 Berlin-Germany, 2023 Brussels-Belgium) In 2022 the Refinery corrosion sessions will take place on <u>Wednesday 31 August</u> in Berlin.

<u>WP Meetings</u> One WP 15 working party meeting in Spring, One meeting at Eurocorr in September in conjunction with the conference, this year it will be on <u>Thursday 1 September 2022 morning in Berlin</u> (possibility of a hybrid meeting to be checked)

Publications - Guidelines

<u>eb site</u>: <u>+and+Petrochemistry+Industry-p-38.html</u>

EFC WP15 spring meeting 24 March 2022



EFC Working Party 15 « Corrosion in Refinery and Petrochemistry »

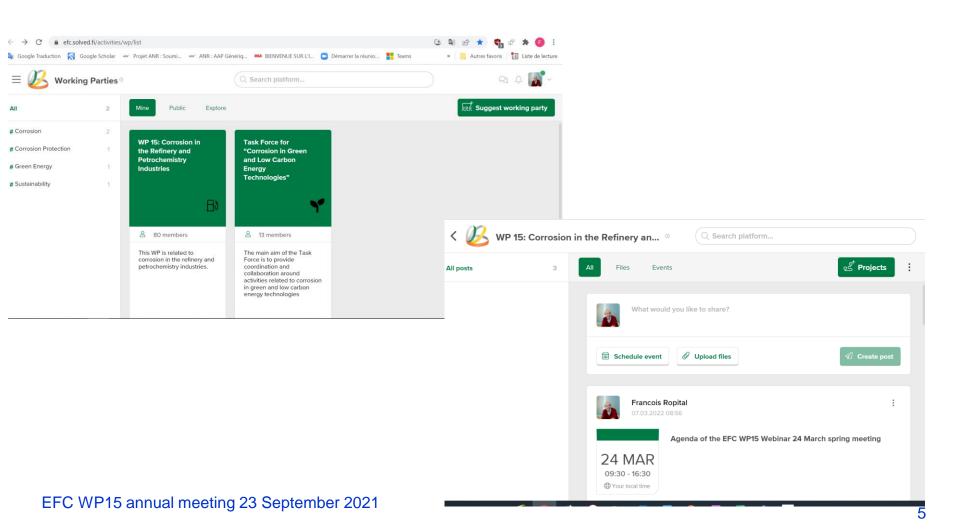
List of the WP15 spring meetings :

Pernis - NL (Shell) Milan -Italy (ENI) Trondheim- Norway (Statoil) Porto Maghera - Italy (ENI) Paris - France (Total) Leiden -NL (Nalco) Vienna - Austria (Borealis) Budapest - Hungary (MOL) Paris - France (EFC Head offices) Amsterdam - NL (Shell) Paris - France (Total) Mechelen - Belgium (Borealis) Leiden -NL (Nalco) Paris - France (Total) Frankfurt - Germany (EFC Head offices) Dalmine - Italy (Tenaris) Roma - Italy (Rina CSM) Zoom meeting



EFC Hub Platform

A Web forum platform on the EFC Hub platform has been created https://efc.solved.fi/activities/wp/list





EFC Hub Platform: CUI Project

EFC CUI Web forum platform:

https://efc.solved.fi/activities/wp/feed/ef91a569-219e-444b-90f8-69c26945cdf7

WP 15: Corrosion in t	Add new item							
osts 3	🖉 Upload files							
	Corrosion Under Insulation EFC publication N°55 - 4th Edition (2024)	:	1					
	Start: 10.09.2021 16:17 End: 30.07.2024 08:33							
	Assign experts							
	These are the next actions you can take depending on your abilities and role, e.g. viewing or editing the full project profile, continuing to feed, making the project visible to other users on All posts Workpackages (21)							
	① Info Image: Feed			WP15/Pub55 CUI 2024 Publication / Appendix J - Case studies	WP15/Pub55 CUI 2024 Publication / Appendix I - Non-destructive examination and testing	WP15/Pub55 CUI 2024 Publication / Appendix H - Use of protection guards	WP15/Pub55 CUI 2024 Publication / Appendix G - Cladding and jacketing materials	WP15/Pub55 CUI 2024 Publication / Appendix F - Types and forms of insulation material
				WP15/Pub55 CUI 2024 Publication / Appendix E - Application of thermally sprayed	WP15/Pub55 CUI 2024 Publication / Appendix D - Coatings	WP15/Pub55 CUI 2024 Publication / Appendix C - additional guidelines on the implementation	WP15/Pub55 CUI 2024 Publication / Appendix B - Quality assurance	WP15/Pub55 CUI 2024 Publication / Appendix A - Cost-economic evaluation
				WP15/Pub55 CUI 2024 Publication / Chapter 8 - Design for the prevention of CUI	WP15/Pub55 CUI 2024 Publication / Chapter 7 - Recommended best practice to mitigate CUI	WP15/Pub55 CUI 2024 Publication / Chapter 6 - Non-destructive examination and testing screeni	WP15/Pub55 CUI 2024 Publication / Chapter 5 - Inspection activities and strategy	WP15/Pub55 CUI 2024 Publication / Chapter 4 - The risk-based inspection methodology fo
EFC WP15 ar	nnual meeting 23 September 2021			WP15/Rub55 CUI	WP15/Pub55 CUI	WP15/Rub55 CUI	WP15/Pub55 CUI	Chapter two



Publications from WP15 - Forum Platform

•EFC Guideline n° 55 Corrosion Under Insulation Editor: Gino de Landtsheer The 3rd revision is available

https://www.elsevier.com/books/corrosion-under-insulation-cui-guidelines/delandtsheer/978-0-12-823332-0

•EFC Guideline n° 46 revision on corrosion in amine units Editor: Johan van Roij is now available

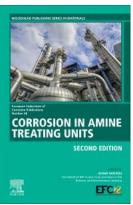
https://www.elsevier.com/books/corrosion-in-amine-treating-units/van-roij/978-0-323-91549-6

 Best practice guideline on corrosion in sea water cooling systems (joint document WP9 Marine Corrosion and WP15)

In progress by a task force

Thank you to all the contributors for their work





EFC WP15 spring meeting 24 March 2022



Advancement of the guideline on corrosion on sea water cooling systems

Chapter	Title	Chapter Leader	Chapter contributor
1	Introduction	Valerie Bour-Beucler	Jean-Nicolas Cordier
	Heat exchanger		
2	systems	Valerie Bour-Beucler	Jean-Nicolas Cordier
3	Sea water environment	Valerie Bour-Beucler	Corrodys
4	Forms of corrosion	Valerie Bour-Beucler	Antoine Surbled
5	Biocide treatments	Valerie Bour-Beucler	Philippe Bleriot
6	Inhibitors	Philippe Bleriot	
8	Materials	Antoine Surbled	
8.1	Carbon steel		Antoine Surbled
8.2	Stainless steels		Dominique Thierry Jonas Howing
8.3	Nickel alloys		Dominique Thierry Angela Philipp
8.4	Copper alloys		Dominique Thierry
	Aluminium, Titanium		
8.5	alloys		Antoine Surbled
8.7	Concrete		Antoine Surbled
9	Corrosion protection	Jian-Zhong Zhang	
	Material selection to		
9.1	avoid galvanic coupling		Jian-Zhong Zhang
9.2	Coatings		Jian-Zhong Zhang
9.3	Cathodic protection		Nicolas Larche Dominique Thierry
	Maintenance and tube		
10	cleaning	Valerie Beucler	Jian-Zhong Zhang Antoine Surbled
	Control monitoring		
11	inspection	Antoine Surbled	

Thank you to all the contributors for their work



If you are not on the list of WP15 members and you want to join you can

•Fill the EFC Friend form: <u>https://efcweb.org/friendsform.html</u>

•Or send an email to <u>francois.ropital@ifpen.fr</u>

EFC Web site :<u>https://efcweb.org/</u>

EFC Hub Platform : <u>https://efc.solved.fi/activities/wp/list</u>

Appendix 3

Cefracor guideline on corrosion in cooling water exchangers

(Francois Dupoiron, Antoine Surbled)

Heat Exchangers Guide

corrosion prevention in cooling water exchangers

A CEFRACOR GUIDE

IDEMAC – François Dupoiron

Aim of the Guide

This guide was initiated five years ago by a CEFRACOR working group with members of specific commissions:

- Inhibitors and water treatments,
- Corrosion in O&G and chemical energy.

Objectives:

-To present synthetic information on corrosion problems occurring on cooling water heat exchangers.

-A compact guide of less than 100 pages with short chapters, accessible to operational personnel and not only to experts.

-Many points are developed in a complementary and detailed way in the appendix (150 pages).

- Sea water cooling is mentionned but not detailled

Status: The project is now 90% complete and the goal is to be proposed for publication by the end of 2022.

General structure of the Guide : HX types , water treatments and Materials

-Presentation of different types of exchangers with their advantages and disadvantages

- Assembly modes and their particularities:
- Sealing and evaluation method
- Mechanical resistance
- Economical aspects

-Materials characteristics and properties and their corrosion behaviour depending the cooling fluid (water):

- compositions and physical parameters (T°C , velocity ...)
- Water treatments (specific chapter)
- Severity evaluation
- Presentation of material solutions including solid , clad , coating
 - carbon steel,,coated carbon steel,
 - -common austenitic stainless steels (types 304 and 316 and variants),
 - austenitic-ferritic stainless steels (duplex),
 - copper and copper alloys,
 - nickel, nickel alloys and bases
 - titanium and titanium alloys.

Structure of the Guide :

Materials :Corrosion sensitivity/ economical aspects / Life cycle cost

For each of the materials solutions,

- Fields of use according to the conditions on the cooling fluid side,
- Effect of the different types of inhibition treatment,
- Corrosion effect of assembly modes , technics and their particularities,
- Galvanic coupling risks
- Economical aspects
- Life cycle cost
- RBI

Detailled structure of the Guide : Damages modes

- The main types of heat exchangers
- 2 Damage modes by exchanger family
- 2.2 The different forms of corrosion
- 2.3 Abrasion and erosion
- 2.4 Erosion Corrosion
- 2.5 Other forms of degradation
- 2.6 Some reminders on the scalling mechanisms
- 2.5 Fouling and biofouling
- 2.6 Problems and recommendations specific to shell and tube exchangers
- 2.7 Problems and recommendations specific to plate heat exchangers

Structure of the Guide : Materials solutions

3 Material solutions

- 3.1 Metallic materials
- 3.2 Composite materials (impregnated graphite)
- 3.3 Non-metallic coatings for tubes and plates
- 3.4 Bimetallic tubes and metallic coatings for tubes and plates
- 3.4.1 Bimetallic tubes
- 3.4.1.1 manufacture
- 3.4.2 Inserts
- 3.4.3 Metal Coatings
- 3.5 Common dimensional characteristics of heat exchanger tubes
- 3.6 Specific instructions for the design of exchangers using cooling water

Strucutre of the Guide : Assembly modes

4 Assembly methods

4.1 Tube exchangers: role of the tube/tube plate connection4.2 Plate heat exchanger assembly

Strucutre of the Guide : CW treatments and material selections

5 Cooling water treatment

6.Selection of materials according to cooling water conditions

- 6.1 Objectives and limits
- 6.2 Environments, metallurgy and associated services6.3 Models
- **7.Life cycle analysis and life cycle costs**

Aim of the Guide : Innovations

- 8 Innovations in heat exchange
- 8.1 Design and manufacture of heat exchange equipment
- 8.2 Low adhesion coatings / conductive coatings / self-healing coatings / improved dirt resistance
- 8.3 Water treatment
- 8.4 Cooling systems
- 8.5 References

Aim of the Guide : Feedback and REX

9. Feedback :

this part contains many feedbacks with observations, failure analysis and recommendations.

This part will remain "open" to be "enriched" with new cases. which will not miss

Appendix A

Supplements Corrosion and scaling

- 1 Vulnerable areas of exchangers
- 1.1 Shell and tube heat exchangers (STHE) and condensers
- 1.2 Plate heat exchangers
- 2 Material behaviour to corrosion in cooling water
- 3.3 Corrosion behaviour of materials in seawater service
- 3.4 Corrosion, corrosion-erosion of copper alloys
- 3.5 Bibliography

Appendix A – Additional information on corrosion

3 Additional information on corrosion

3.6 Conditions for the appearance of calcium carbonate

- 3.7 Interaction between the CaCO3 nuclei and the walls
- 3.8 Growth of deposits on the walls
- 3.9 Influence of suspended matter and algae
- 3.10 Influence of metal ions and oxidants
- 3.6 Influence of the water heating method
- 3.7 Principle of antiscalant treatments
- 3.11 Evaluation of the effectiveness of treatments
- 3.12 Examples of antiscalant treatments
- 3.13 Evaluation of the scaling power of a circuit
- 3.14 Conclusion
- 3.15 Bibliography

Appendix A

4 Reminders on the Ryznar and Langelier indices4.1 Limitations of the Ryznar and Langelier methods4.2 Conclusion

Appendix B – General properties of materials

Appendix B: General properties of materials

- 1 General material properties
- 1.1 Cost and availability
- 1.2 Mechanical and physical properties
- 1.3 Environment
- 1.4 Suitability for the intended service
- 2 Metallic materials
- 2.1 Influence of metallurgy, microstructure and surface condition on corrosion behavior
- 2.2 Structure of metallic alloys
- 2.3 Ferrous alloys
- 2.4 Non-ferrous metals and alloys
- 2.5 Properties of alloys
- 2.6 Bibliography

Appendix C: Heat exchange, hydrodynamics, vibrations, cavitation

- 1 Heat exchange in the design of heat exchangers
- 1.1 Objectives
- 1.2 Reminder on heat exchangers used in cooling water service
- 1.3 Reminder on heat transfer
- 1.4 Heat Transfer Analysis
- 1.5 Design of a Heat Exchanger
- **1.6 Nomenclature**
- 1.7 References
- 2 Thermomechanics of Fluids

Appendix C : thermomechanics of fluids

- 2 Thermomechanics of Fluids
- 1.1 Definition of a Fluid
- **1.2 Fluid Behavior**
- **1.3 Hydrodynamics**
- **1.4 Elements of Rheology**
- **1.5 Balances**
- 1.6 General Formulation of the Flow Problem
- **1.7 Representation of the Balance Equations**
- 1.8 Hydromechanical Behavior of a Fluid in a Tube
- 1.9 Nomenclature
- 1.10 References

Appendix C FIV and cavitation

3 Flow-induced vibrations in shell-and-tube heat exchangers, (FIV)

- 3.1 Flow-induced vibrations, Principles
- 4.3 Vibration prevention
- 2.3 Anti-vibration devices
- 4.4 Modeling and Prediction of FIV
- 4 Cavitation
- 4.1 Definition
- 4.2 Origins
- 4.3 Forms of cavitation
- 4.4 Theory, mechanism and factors
- 4.5 Morphology

Appendix 4

A case study of corrosion in cooling water treatment

(Federico Ciocca, Alessandro Vanacore)



EFC Working Party 15 Spring "Corrosion Refinery and Petrochemistry Industry" Meeting - 24th March 2022

Corrosion in cooling water systems - A case study of corrosion in cooling water treatment



During a field inspection it was observed that the tower water treatment was carried out incorrectly

- Visual inspection of the tank → corrosion inside the tank and damages on the pumps
- Visual inspection of the line → presence of many perforated carbon steel curves
- Failure analysis \rightarrow in order to establish the cause of curve perforation
- Recommendations to mitigate the problem

A case study of corrosion in cooling water treatment

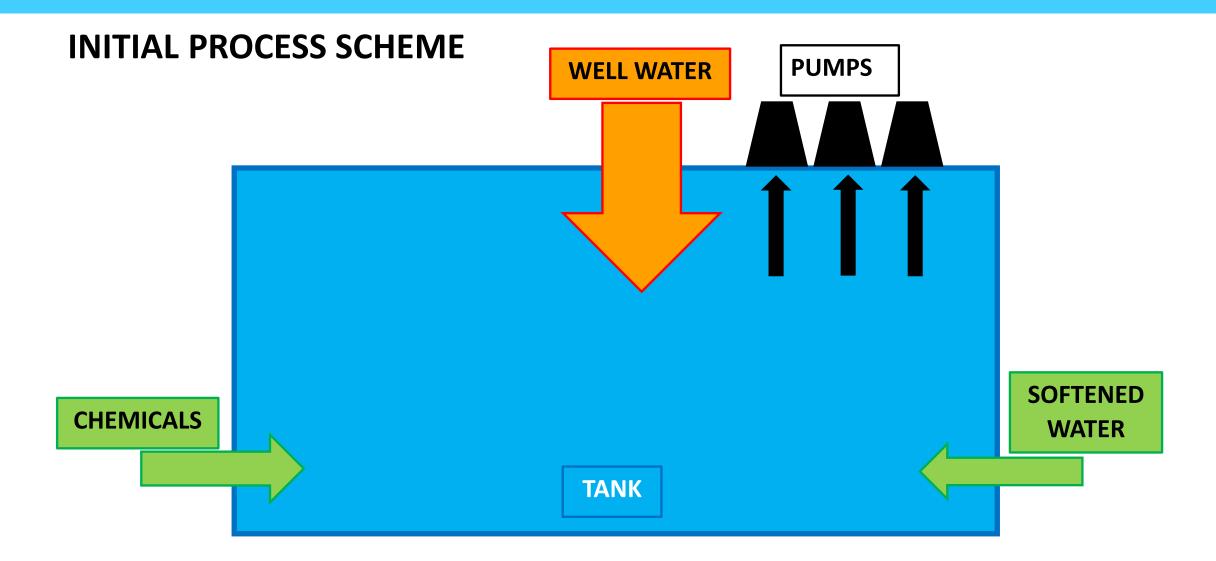


PROCESS WATER COLLECTION SYSTEM:

- TANK: process water storage
- CHEMICALS: improve water quality
- **SOFTENED WATER:** pre-treated to remove salts
- WELL WATER: water reinforcement
- **PUMPS:** take water for the plant circuit

A case study of corrosion in cooling water treatment





A case study of corrosion in cooling water treatment



PROBLEMS:

- Well water inlet → too close to pumps
 → often greater then softened water
- Chemicals \rightarrow not directed correctly
 - \rightarrow inlet counts carried out only on softened water
- No mixing system inside the tank







WELL WATER INJECTION

CHEMICALS INJECTION



PROBLEMS \rightarrow **SOLUTIONS**

• Well water inlet → too close to pumps → Placed further (design change)

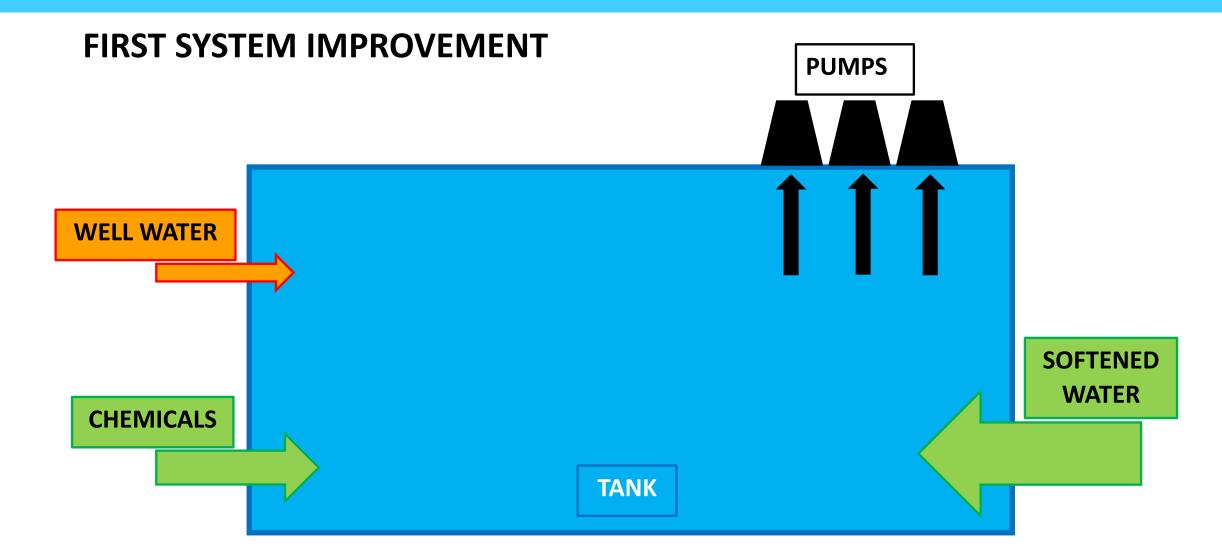
 \rightarrow often greater then softened water \rightarrow Try to reduce well water inlet

- Chemicals → not directed correctly → Repositioning of the sprinklers

 → count carried out on softened water → Increasing dosage according to inlet well water
- No mixing system inside the tank \rightarrow New precaution could improve mixing in the tank

A case study of corrosion in cooling water treatment Anticorrosione

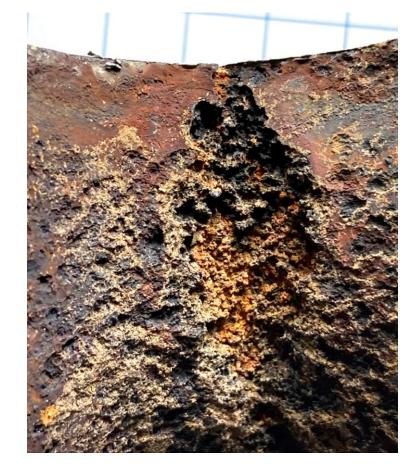






...HOWEVER... Passing corrosion on intrados curves \rightarrow









→ FAILURE ANALYSIS



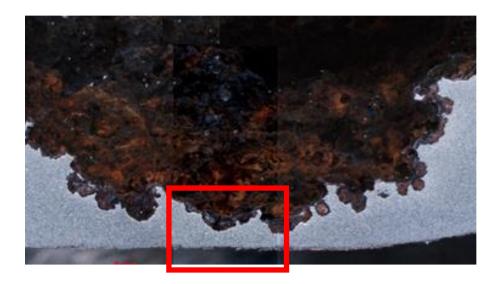
EXTRADOS: NO damages on internal / external surface

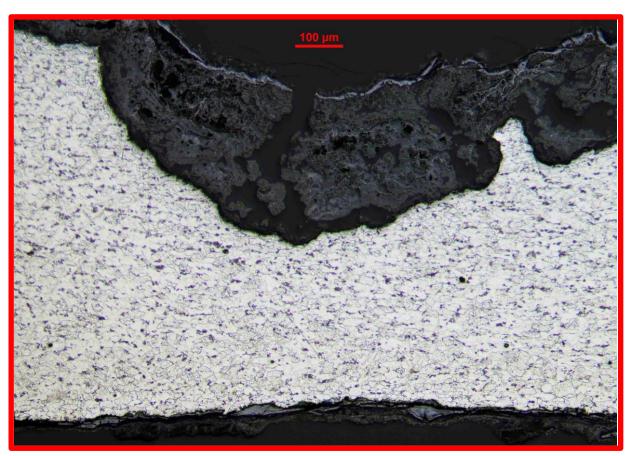
INTRADOS:

- NO damages on external surface
- Passing corrosion on internal surface



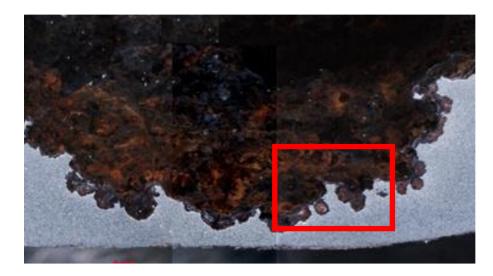
→ FAILURE ANALYSIS → Curve intrados (detail X100)

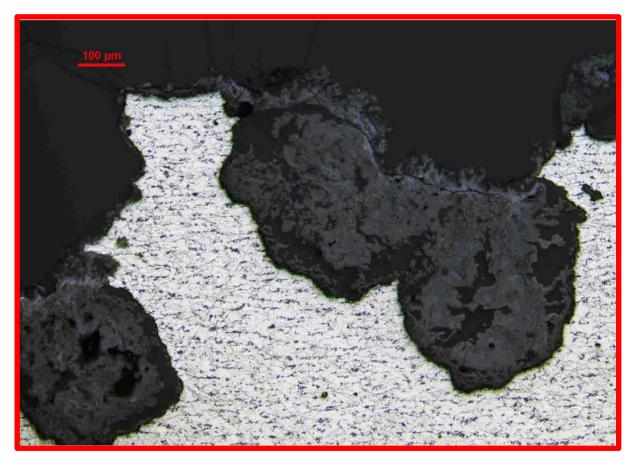






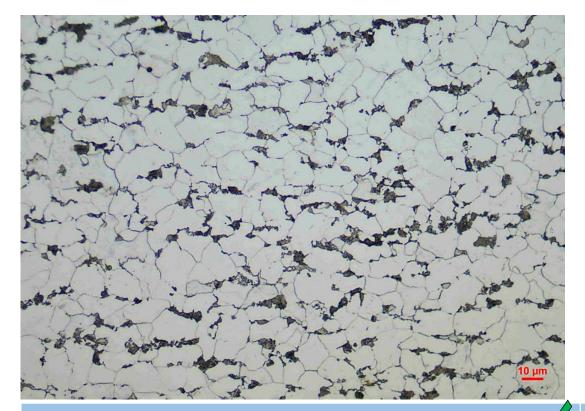
→ FAILURE ANALYSIS → Curve intrados (detail X100)







\rightarrow FAILURE ANALYSIS \rightarrow Curve intrados



METHOD	HV 1
MEASURED VALUES	130 HV 138 HV 154 HV
AVERAGE HARDNESS	141 HV

Crystalline microstructure (X500) 💊

Hardness Test



 \rightarrow FAILURE ANALYSIS \rightarrow CONCLUSIONS

- Crateriform corrosion → Incorrect water treatment
- Microbiologically induced corrosion (MIC) → Accelerate corrosion rate (bacteria count X10 max)
- Why only intrados ? → more turbolent flow



- \rightarrow FAILURE ANALYSIS \rightarrow Recommendations
- Crateriform corrosion
 → Improvements (seen previously)
- MIC → Continuous biocidal treatment of tower water with hypochlorite and weekly monitoring the bacterial count (maximum recommended value < 10³ ufc/ml)
- Install corrosion test samples in the circuit, to assess the aggressiveness of the water, and monthly monitoring the weight loss and visual appearance.



IN CONCLUSION:

BAD DESIGN, AND INCORRECT TREATMENT OF TOWER WATER CAN ALSO LEAD TO FAILURES IN THE CIRCUIT

APPROPRIATE VISUAL INSPECTIONS AND THICKNESS MEASUREMENTS COULD DETECT THE PROBLEM BEFORE THE FINAL FAILURE

APPROPRIATE WATER ANALYSIS AND CORROSION TESTS IN THE CIRCUIT CAN GUARANTEE THE CONSTANT QUALITY OF THE WATER USED EFC Working Party 15 Spring "Corrosion Refinery and Petrochemistry Industry" Meeting - 24th March 2022

A case study of corrosion in cooling water treatment

MANY THANKS TO ALL THE ATTENDERS





Alessandro Vanacore

Capo Dipartimento Controlli non Distruttivi 3° Livello VT-PT-MT-ET-UT-PAUT-TOFD-AE-LT UNI EN ISO 9712 2° Livello RE-ME-TT UNI EN ISO 9712 Ispettore PED – ambito di Approvazioni 3.1.3 – numero identificativo 150 in collaborazione con ICEPI

Federico Ciocca

Tecnico metallografo – Failure Analysis 2° Livello RE-ME UNI EN ISO 9712

Donegani Anticorrosione s.r.l.

Via G. Fauser, 36/A 28100 – Novara (NO) Tel. 0321/690429 - Fax 0321/696696 Mobile 0039/342 3233032



Appendix 5

Corrosion in biorefinery production: working together towards sustainability

(Namurata Pälsson)

Corrosion in Biorefinery Production: Working Together Towards Sustainability

EFC WP15 Meeting 24 March 2022



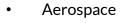
Member programs within corrosion

(MRC – Member Research Consortium)

- Automotive corrosion
- Surface technology
- Corrosion protection
- Corrosion in pulp & paper industry
- Corrosion of polymer materials
- Brass Alloys
- Corrosion and cathodic protection in soil
- Corrosion in Biorefinery Production



MRC in France



- Coil coating
- Corrosion in oil & gas production
- Corrosion off-shore
- Paints and linings for steel structures
- Hydrogen

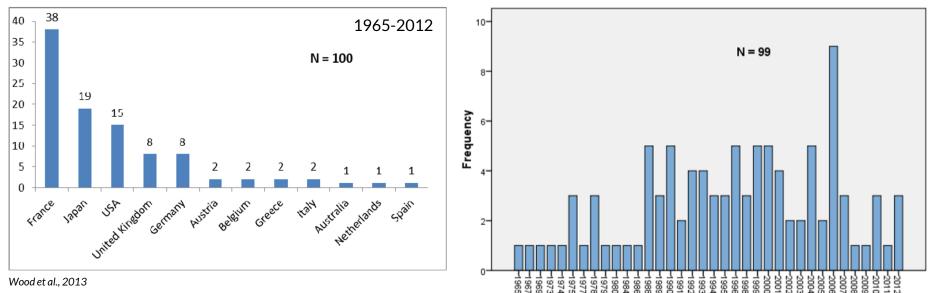


Do we really need to worry?

JRC SCIENTIFIC AND POLICY REPORTS

Corrosion-Related Accidents in Petroleum Refineries

Lessons learned from accidents in EU and OECD countries



Why we take these steps

- Possibility of corrosion in biorefinery production is not zero.
- Service conditions for biorefinery processes are highly complex.
- Knowledge related to the processes and material selection is crucial to mitigate or predict corrosion of components used in the challenging environments.
- Preventive maintenance!

Actions

- Researchers
- Scientists
- Material producers
- Biorefinery plant operators



https://www.ri.se/en/what-we-do/networks/mrc-biorefinery

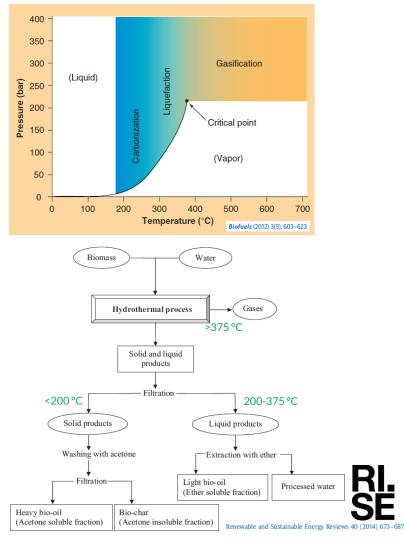


MRC on Corrosion in Biorefinery Production

Based on scientific research, as well as strong collaboration among key players in biorefinery production, including plant operators, material producers, and experts on materials and corrosion, Member Research Consortium (MRC) Corrosion in Biorefinery Production will help its members with corrosion issues.

Actions

- Experimental tests based on a literature study
- Temperature
 - Hydrothermal carbonization: 200 °C, 15 bar
 - Hydrothermal liquefaction: 300 °C, 90 bar
- Additive
 - HCI pH 3
- Exposure time
 - 500 h



Corrosion resistant alloys

- nominal composition

Alloys/ Elements	С	Si	Mn	Р	S	Cr	Ni	Мо	Cu	N	PREN
654 SMO	0.01		3.5			24	22	7.3	0.50	0.50	56
Sanicro [®] 35	≤0.030	≤0.5	0.8	≤0.030	≤0.020	27	35	6.5	0.2	0.3	53
Alloy 625	0.10	0.50	0.50	0.015	0.015	20-23	≥58	8-10	-	-	52
254 SMO	0.01					20	18	6.1	0.71	0.2	43
Sanicro [®] 28	≤0.020	≤0.7	≤2.0	≤0.020	≤0.010	27	31	3.5	1.0	≤0.1	40
316L	0.02					17.2	10.1	2.1	-		24

<u>Pitting Resistance Equivalent Number = Cr + 3.3Mo + 16N</u>

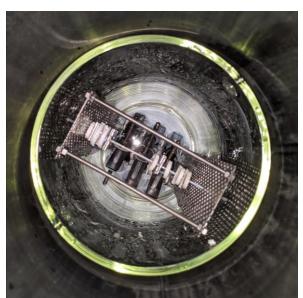






Testing conditions



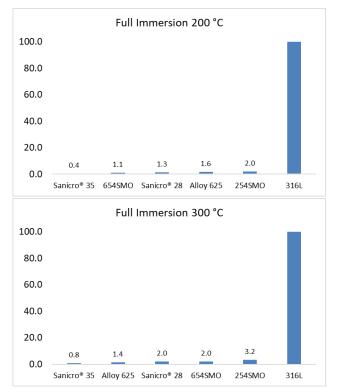


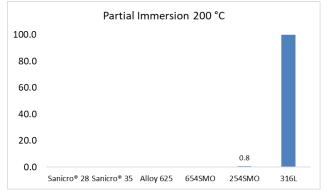
Partial immersion

Full immersion

RI. SE

Corrosion rate – relative percentage





Partial immersion for 300 °C is not available.

The test at 300 °C will be repeated.



Summary of the results

• Effect of chemical compositions

 Corrosion of Sanicro[®] 28, Sanicro[®] 35 654SMO, Alloy 625 and 254SMO were in the same range and significant lower than that of 316L.

• Effect of exposure conditions

 Samples exposed to two-phase environment exhibited significantly higher corrosion rate than those exposed fully in the liquid phase.

• Effect of testing temperature

- Testing temperature of 300 °C exhibited much more aggressive results than testing at 200 °C.
- Effect of applied stress
 - U-bends did not show crack after exposure.
 - Partial immersion of U-bends is of interest for future work.

Next steps

- Effect of chloride on corrosion of different alloys with and without acid at high temperature and pressure
 - Literature study
 - Knowledge gap
 - Effect of organic and inorganic salts
 - Experimental work
 - Different sources of chloride based on different processes





Appendix 6

Corrosion with vegetable oils used for the production of biofuels

(Jean Kittel)

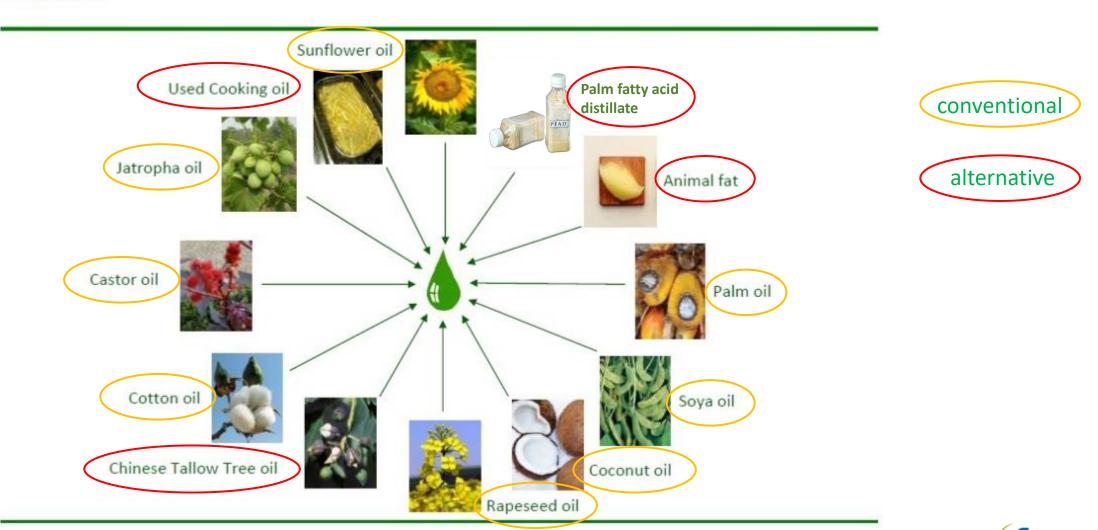
CORROSION IN VEGETABLE & WASTE OILS USED FOR THE PRODUCTION OF BIO-FUELS

<u>Fouad Andari</u>^a, Jean Kittel^a, Joana Fernandes^a, Benoît Ter Ovanessian^b, Marion Frégonèse^b, Nathalie Godin^b, François Ropital^{a,b}

^a IFP Energies Nouvelles, Rond-Point de l'échangeur, Solaize, France 69360
^b University Lyon, INSA-LYON, MATEIS UMR CNRS 5510, Bât L. de Vinci, 21 Avenue Jean Capelle, F-69621 Villeurbanne cedex, France







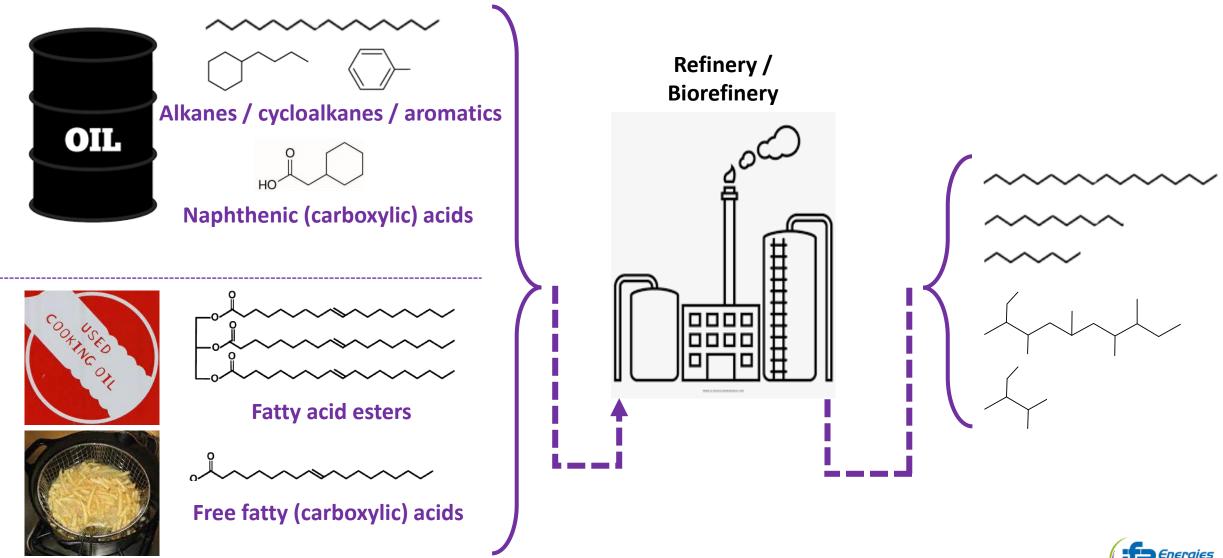
SOME FEEDSTOCK IN BIOFUEL PRODUCTION

Feedstocks



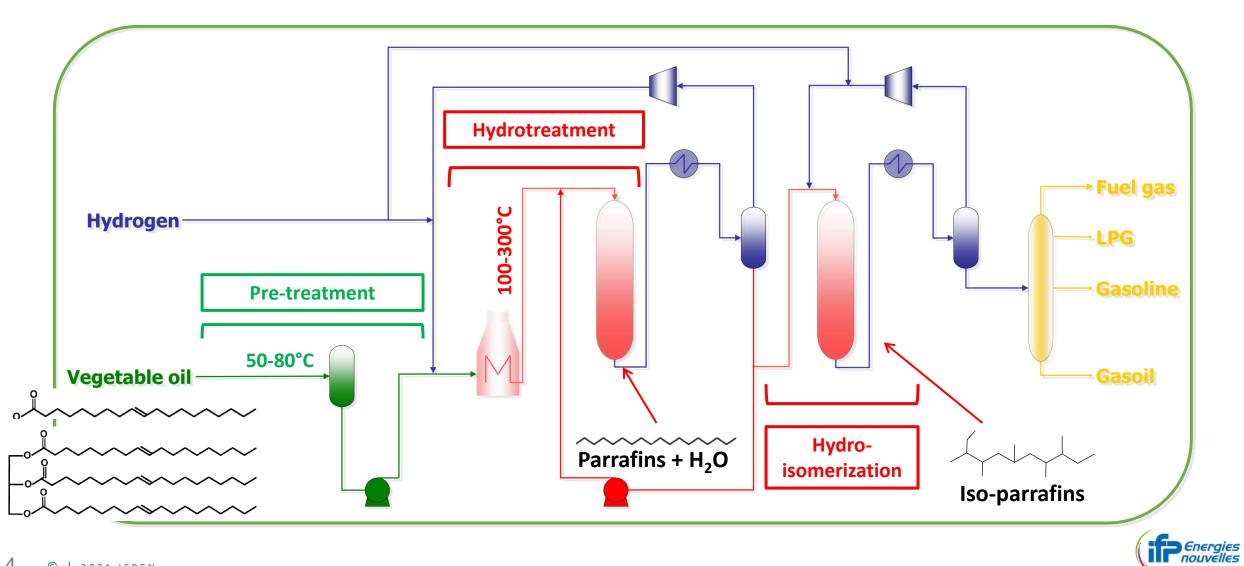
VEGETABLE OILS VS CONVENTIONAL CRUDE OIL





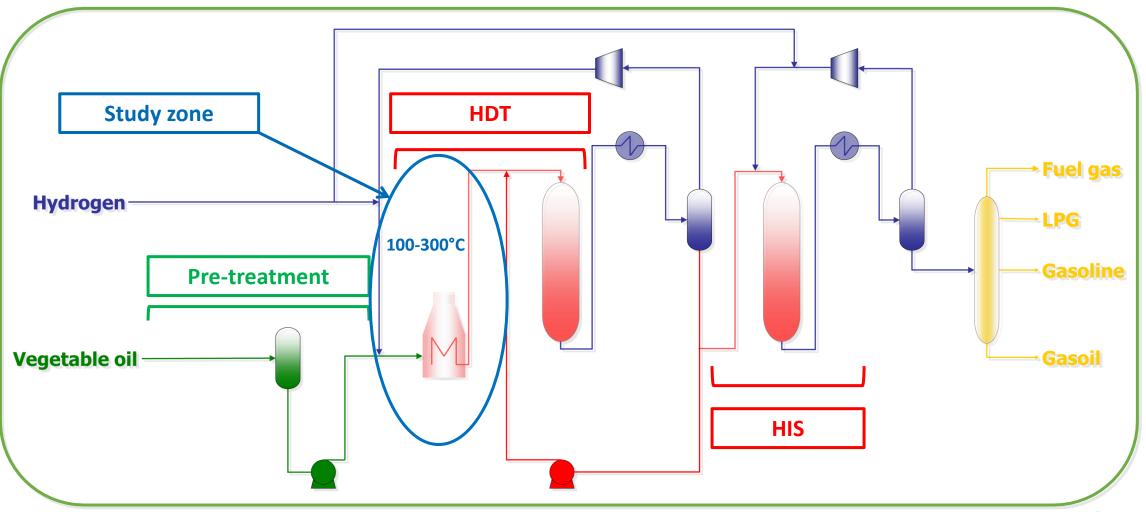


REFINING VEGETABLE OILS



Renewable energies







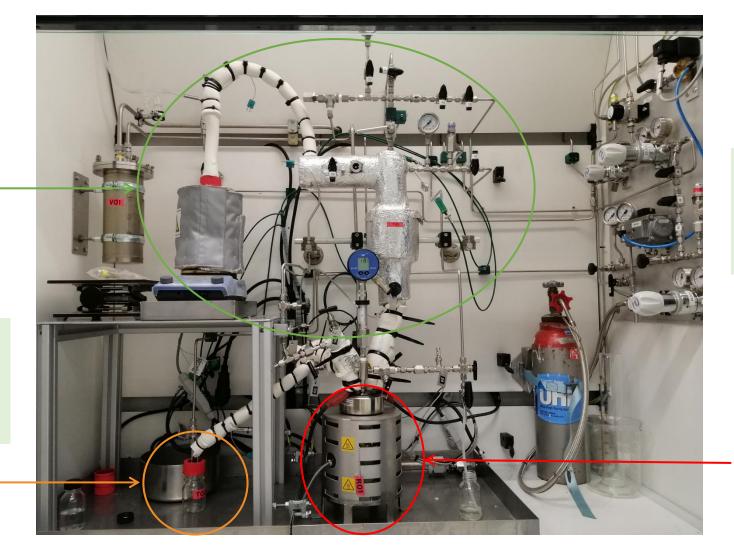
EXPERIMENTAL TEST UNIT

Oil conditioning and transfer

Post-test analysis

- \circ Infrared
- Simulated distillation
- Dissolved metal (ICP)

Sampling point



Weight-loss coupons o 316L

- o 1.25Cr/0.5Mo
- Carbon steel

Autoclave V = 600ml $T^{\circ}max = 500^{\circ}C$ $P^{\circ}max = 138bar (H_2/N_2)$



• Corrosion tests at 220 °C for 5 days

weight loss coupons (carbon steel / low alloy steel / stainless steel)
 post test solution analysis

OPart 1

Tests with 10 industrial feeds to detect the most influent parameters

OPart 2

Tests with model solutions prepared with a non corrosive oil and pure oleic acid



PART 1 – TESTS IN INDUSTRIAL FEEDS COMPOSITION OF TESTED OILS

		Vegetable oils				Animal	based	By-products or wastes			
		Refined Rapeseed	Refined Sunflower	Refined Soja	Refined Palm	Animal fat	Fish oil	WCO	PFAD	TOFA	DTO
Acid value	[mg _{KOH} /g]	0.06	0.06	0.06	0.16	10.2	4.6	16	185	196	192
Peroxide index	[meqO ₂ /kg]	0.6	2.1	0.7	1.1	13.4	3.4	1.2	1.2	7.2	-
Water content	[mg/kg]	150	170	150	100	709	1000	3310	1468	240	-
lodine index	[g/100g]	115	126	132	53.5	78	136	87	61	146	-

- 10 industrial feeds
- acid values from 0 to 200 mg_{KOH}/g
- different types of fatty acid esters (C16 to C22)



PART 1 – TESTS IN INDUSTRIAL FEEDS CORROSION RATE

Distilled Tall Oil wastes 192 **Tall Oil Fatty Acid** 196 **By-products or** Palm Fatty Acid Distillate 185 **Used Cooking Oil** 16 **Animal based** Animal fat (purified) 10.2 Fish oil 4.6 0.16 **Refined Palm** Vegetable oils 0.08 **Refined Colza Refined Sunflower** 0.06 **Refined Soja** 0.06 10,0 100,0 1000,0 1,0 10000,0

■ 316L ■ A387Gr11 ■ CS1018

Corrosion rate $(\mu m/y)$

• 316L is always immune

- Corrosion of CS and LAS increase with acid value
- At 220 °C, corrosion rates above 0.1 mm/y are obtained when the acid value exceeds 4 mg_{KOH}/g



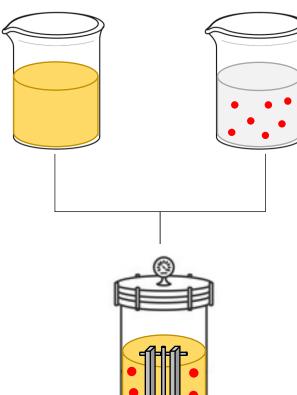
Renewable energies

Acid value (mg_{KOH}/g)

PART 2 – TESTS IN MODEL SOLUTIONS PREPARATION OF THE SOLUTIONS

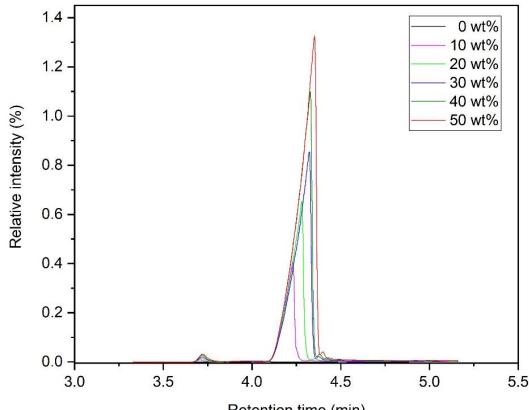
Colza oil

Oleic acid



mass % of oleic acid	acid value (mgKOH/g)
0	0.8
10	19
20	38
30	58
40	77
50	97
70	152

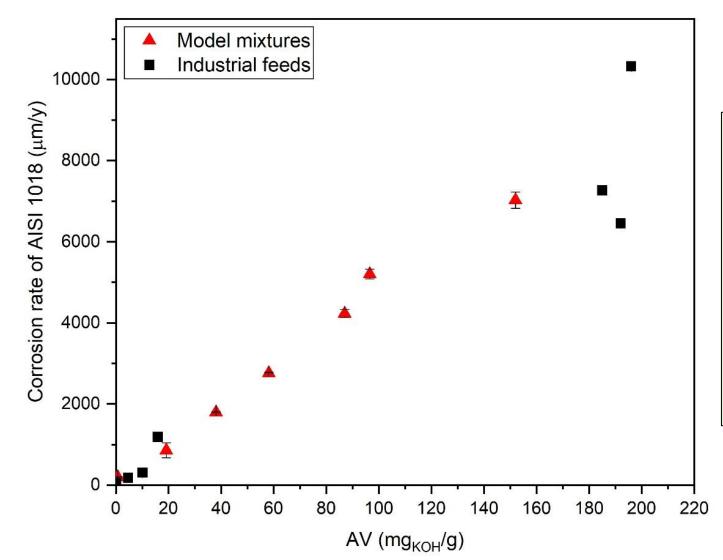
Titration of FFA by SIM-DIS



Retention time (min)



TESTS IN MODEL SOLUTIONS 1/ CORROSION RATE VS ACID VALUES

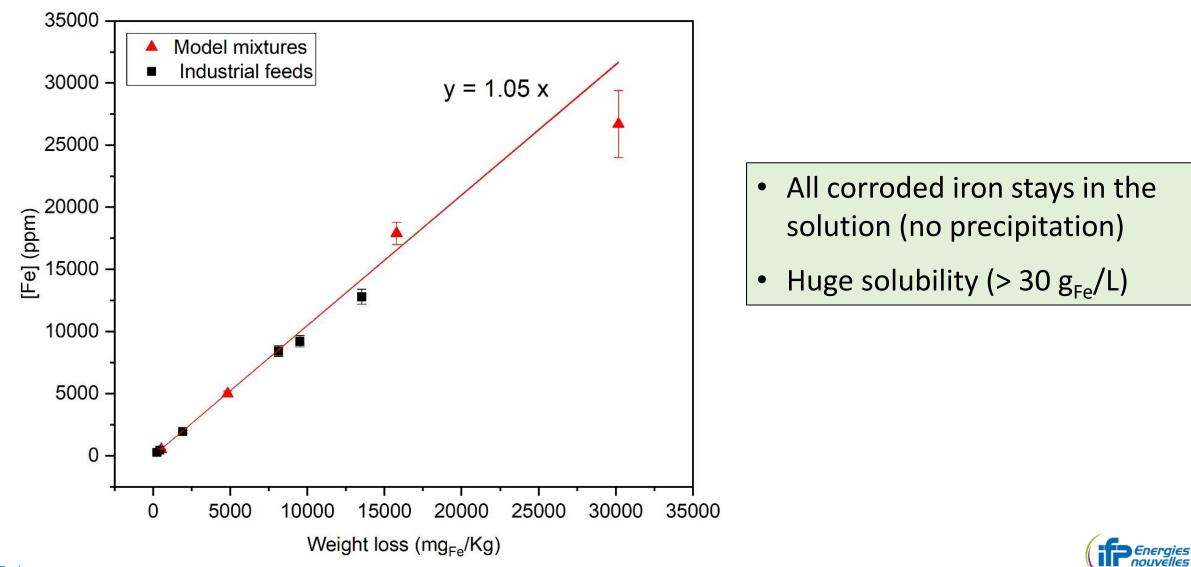


Renewable energies

- Impact of acid value is confirmed
- Linear evolution of carbon steel corrosion rate with acid value
- Same curve for model and industrial solutions



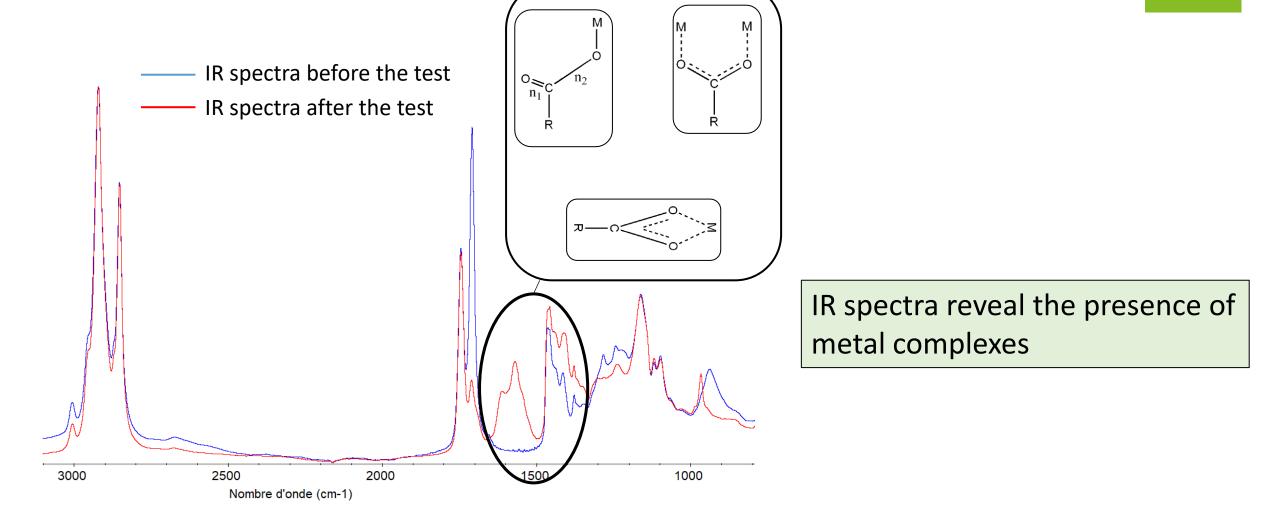
TESTS IN MODEL SOLUTIONS 2/ DISSOLVED IRON



energies

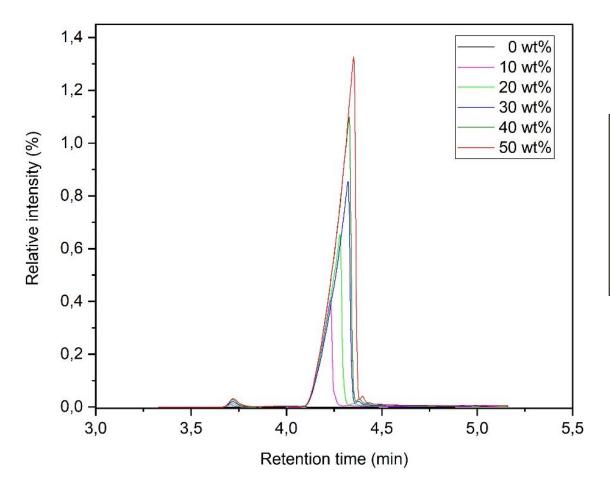
TESTS IN MODEL SOLUTIONS 2/ DISSOLVED IRON

Renewable energies





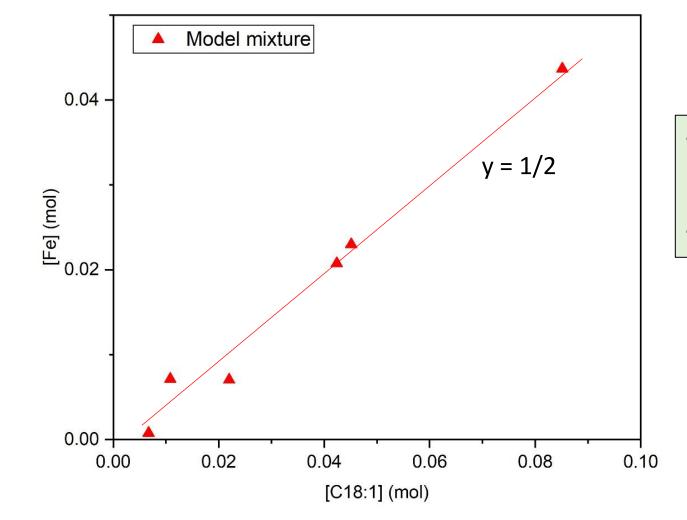
TESTS IN MODEL SOLUTIONS 3/ CONSUMPTION OF FREE FATTY ACIDS



- Free fatty acid content measured before / after each test with SIM-DIS analysis
- Acid consumption correlated with iron dissolution



TESTS IN MODEL SOLUTIONS 3/ CONSUMPTION OF FREE FATTY ACIDS



- The amount of corroded metal is well correlated with the consumption of FFA
- 2 moles of acid react with 1 mole of Fe





- Carbon steel and low alloy steel show linear evolution of corrosion rates with acid value
- The linear trend is similar for industrial feeds and model solutions
- At 220 °C, the limit of 0.1 mm/y is reached when the acid value exceeds a few mg_{KOH}/g
- The amount of corroded metal is proportional (factor 1/2) to the quantity of consumed free fatty acid
- The huge solubility of iron is explained by the formation of complexes involving the carbonyl group of FFAs



Appendix 7

Corrosion overview in biorefineries

(Marco de Marco)

Overview of corrosion in Biorefinery

M. De Marco - IIS



"...use of vegetable oils for motor fuel may seem insignificant today, but such oils can become, over time, as important as modern-day petroleum and coal derivatives..."

Rudolf Diesel, 1912



Origins

Biodiesel was originally produced by E. Duffy and J. Patrick 40 years before the invention of the diesel engine.

In 1893, **Rudolf Diesel** himself ran the first of his engines using peanut oil as a fuel.

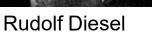
The recent interest in biodiesel was born in 1991 with the commissioning of the **first production plant** on an industrial scale in Austria.

Since then, numerous plants have been started up especially in the European area In 2005, more than 3,500,000,000 liters of biodiesel were produced worldwide.

Jatropha Curcas and seeds







Feed stock - Biomass

Biomass means "the biodegradable fraction of products, waste and residues of biological origin from agriculture (including plant and animal substances), forestry and related industries, including fishing and aquaculture, as well as the biodegradable part of waste industrial and urban".

Biofuels are fuels that derive from biomass and are opposed to fuels of fossil origin (.. in fact, they too derive from biomass, but no longer living for a long time ...).

Examples of biomass used as a renewable base for fuels are wood, rod, corn stalk, and other agricultural waste, sugar, corn starch, soybean, rapeseed, palm oil, pongamia and jatropha, algae, oils and fats animals also waste, etc. etc.



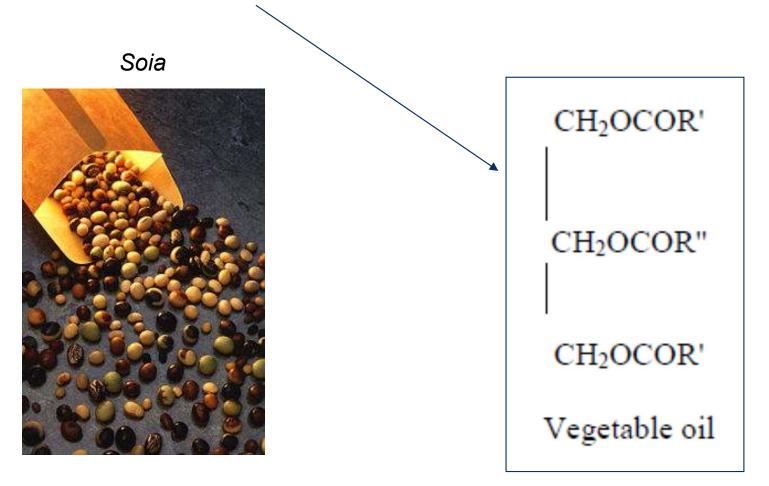




Feed stock - Biomass

Biomasses are mainly composed of carbon, hydrogen and oxygen atoms with the presence of sulfur, nitrogen, phosphorus, other metals and chlorine.

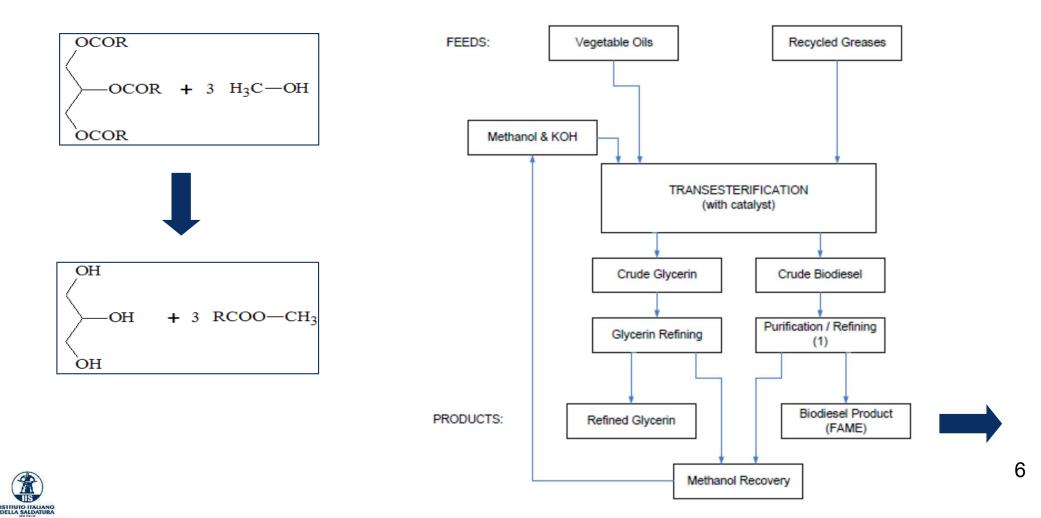
e.g. cellulose, lignin, triglycerides, fatty acids, glycerol esters.



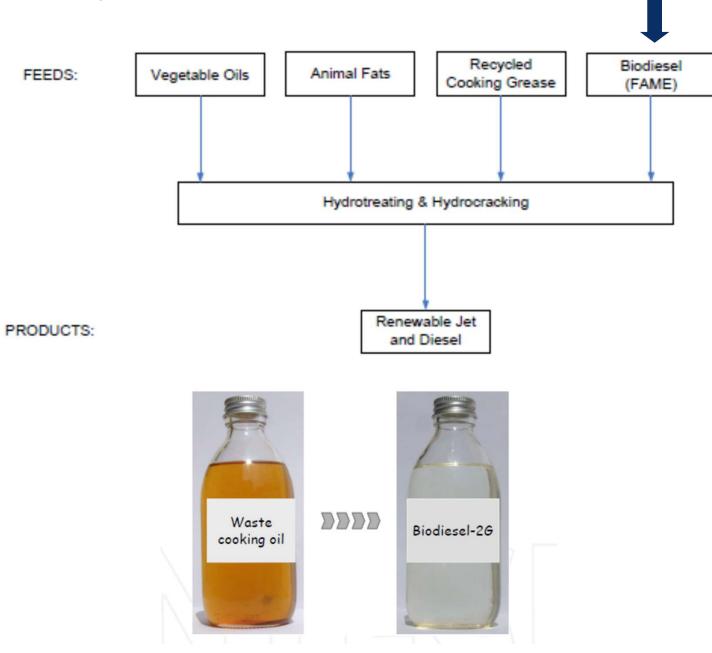


The terminology Biodiesel generally defines **mono-alkyl esters of various fatty acids** (Fatty Acid Methyl Ester - **FAME**, VME - Vegetable Methyl Ester) obtained by trans-esterification reaction of biolipids with alcohol and catalyst (e.g. soda, potash).

 \rightarrow First generation **Biodiesel**



Need to create **"drop-in" renewable fuels** (second generation) practically interchangeable with those of fossil origin.





Production - Decomposing and reassembling

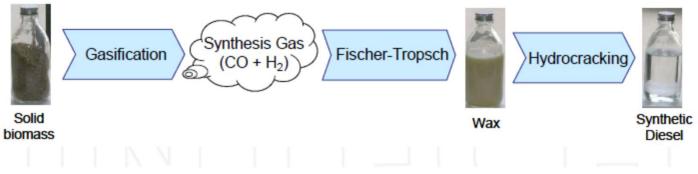
The molecules of biofuels are smaller than the originals from which they derive: rupture reactions (**decomposition**).

This is followed by a phase of **synthesis**, **purification and transformation (reconstruction**) into purer and more functional mixtures.

Biomass Feeds	Biomass Deconstruction Steps	Synthesis/Purification Steps	Biofuel/Bio-based Chemical Products	
Lignocellulosic Biomass Ro	outes			
Wood	Gasification to CO & H ₂	Fischer-Tropsch Mixed Alcohols Methanol to Ethyl Acetate to Ethanol Fermentation	Renewable Jet Renewable Diesel Ethanol	
Wood Waste Corn Stalks Corn Cobs Agricultural Waste	Strong Acid Hydrolysis	Fermentation	Ethanol Butanol Renewable Gasoline Renewable Xylene	
Switchgrass Energy Cane MSW (newspapers, grass	Weak Acid Hydrolysis	Fermentation	Butanol Isobutanol	
clippings, etc)	Enzymes (biocatalysts)	Fermentation	Ethanol	
	Weak Acid Hydrolysis & Enzymes	Fermentation Fermentation-Acetic Acid- Ethyl Acetate-Hydrogenation	Ethanol	
Pyrolysis		Hydrotreating	Renewable Gasoline Renewable Jet Renewable Diesel Renewable Xylene	
Plant Oil & Fat Based Route	es			
Triglycerides: Plant Oils	Chemical transesterification with	N/A	Biodiesel	
 Canola Soy Palm Jatropha Algae 	methanol to fatty acid methyl esters (FAME) using an acid or base catalyst	Hydrogenation and hydrocracking	Renewable (drop in) jet & diesel	
Animal Fats Grease from restaurants Slaughterhouse waste Rendering plants 	High temperature hydrolysis	Hydrogenation		



Certain reactions and certain processes present in the production of **biofuels/renewable fuels** are familiar to corrosion and materials engineers working in the refining field (hydrotreatment, hydro-conversion, isomerization, distillation, etc.).



Raw materials and intermediates change!

"Fossil" refinery: hydrophobic hydrocarbons with sulfur (sulfides, mercaptans, etc.), nitrogen compounds and small quantities of oxygen.

By-products from processing: hydrogen sulfide, ammonia and only small quantities of water.

Bio-based fuels: starting with species with a high oxygen content (carbohydrates, triglycerides, Free Fatty Acids – FFA, etc.). *Products and by-products*: oxygenated species such as alcohols, CO₂, organic carboxylic acids and water as a by-product. High Acidity Numbers (TAN)

The presence of **water** increases corrosion problems.



Corrosion Issues

The widespread presence of **aqueous phase** makes the process fluids in any case potentially more corrosive than hydrocarbons of fossil origin.

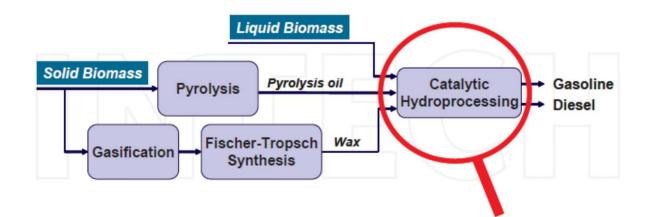
H₂O solubilizes numerous corrosive agents present

- \rightarrow Organic acids
- \rightarrow Inorganic acids
- $\rightarrow CO_2$
- \rightarrow Chlorides

and promotes MIC.

The refinement process by hydrotreating allows to eliminate the oxygenated species (organic acids) and refine the molecular structure (saturation, isomerization, etc.).

```
✓ "Drop-in" fuels – Renewable Fuels - RF
```





The literature reports evaluations concerning the corrosion problems in the following phases of the life cycle of biofuels:

- Raw materials: corrosion in tanks containing vegetable oils.
- Finished products: corrosion in transport systems and tanks for biofuels.
- **Combustion:** corrosion in combustion products (internal combustion engines, power plants, etc.).

To the present date, there are **gaps** in the **assessments of corrosion** and **material selection issues** in the intermediate stage of production.

The variability of the processes, often covered by patents, makes the situation more complicated.



RF production– Corrosion mechanisms

The different stages of RF production are characterized by numerous potential corrosion and damage mechanisms to be considered when selecting materials and define inspection intervals (1)

- \rightarrow **Organic acids** in the presence of condensed water
- →High temperature organic acids (and FFA) in the absence of condensed water (T> 100 ° C)
- \rightarrow CO₂ in the aqueous phase (due to Hydrodecarboxylation reactions HDC)
- \rightarrow **Chlorides** in aqueous solution (pitting and SCC)
- \rightarrow High temperature hydrogen attack (HTHA API 941)
- \rightarrow Corrosion and alkaline SCC in soda and potash (catalysts)
- →Corrosion by mineral acids (sometimes used as catalysts in the decomposition phase of biomass)

The presence of organic acids in low T anhydrous fluids can become critical even in the initial absence of water \rightarrow **bio-based fuels are hygroscopic!**

(1) Da Impact of Organic Acid on Materials Selection for Biofuels and Bio-Based Chemical Plants -Cathleen A. Shargay, Karly Moore and Marty West



Corrosion Issues - Feedstock

		·		Oil Properties				Corrosion Rates (mm/yr)			
		Pyrolysis Oil	Biomass Feed Stock	Total Acid Number (TAN)	Formic Acid Conc. (ppm)	Acetic Acid Conc. (ppm)	CS	K21590	S40900	S30403	S31603
		1	Oak	86	2400	19000	0.9/2.4	0.2 / 0.2	0.1/	0.0 /	0.0 / 0.0
		2	Mixed Hardwoods	108	7756	40668	2.6/2.4	3.3/3.3	0.6 / 0.6	0.0/0.0	0.0 / 0.0
		3	Forest Residue	66	6490	7778	2.8/3.1	4.0 / 4.2	0.7 / 0.0	0.0 / 0.0	0.0 / 0.0
Treated		4	Wood	14			0.5/0.4	1.2 / 0.1	0.8 / 0.1	0.0/0.0	0.0 / 0.0
with H ₂	×	5		68			2.6/0.2	2.4/2.6	0.0 / 0.0	0.0/0.0	0.0 / 0.0
		6	Switch- grass	58.5			0.6/0.6	1.4 / 1.5	0.8 / 0.8	0.0/0.0	0.0 / 0.0
		7		0.23 (Note 1)			0.0/0.0	0.0 / 0.0	0.0 / 0.0	0.0 / 0.0	0.0 / 0.0

Medium	Corrosion Coupon Results (mm/yr)	Average Corrosion Rate (mm/yr)	
B99 – Biodiesel with 1% of 3% NaCl	0.09, 0.07, 0.14	0.10	
B100	0.03, 0.02, 0.01	0.02	

T Amb	
TAN < 0.3 mg /gr	



Corrosion Issues - Feedstock

MIC cases on Soybean oil pipeline.



Processing - Organic acids in presence of condensed water

In several areas of the plants for RF production, conditions may occur in which a **condensed aqueous phase + organic acids** is present.

CO₂ and chlorides may also be present.

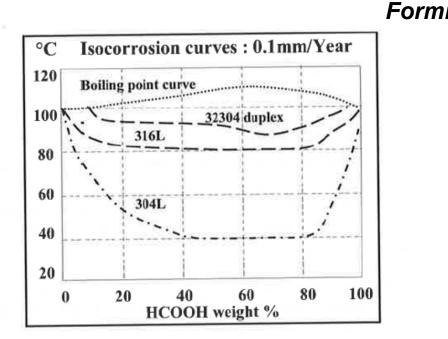
pH of pure water @ T=25 ° and 100 ppm acid				
Acid pH				
Formic	3,9			
Acetic	4,2			
Propionic	4,4			
Butanoic	3,8			
Sulfuric	3			

Even a few ppm of organic acids can induce corrosion on carbon steel



Stainless steels perform better.

Especially with higher chromium content with molybdenum (316, 2205)



			Dearate
cid .	×		
	Corro	sion Rate (m	nm/yr)
ACID CONCENTRATION	\$30400 ^(A)	\$31600 ^(A)	S31600 ^(B)
1.0	0.17	0.09	
5.0	0.77	0.04	
10.0	1.33	0.26	
20.0	1.89	0.27	
40.0	3.40	0.20	
50.0	4.20	0.50	0.46
60.0	3.40	0.46	
70.0	3.97	0.48	0.64
80.0	4.20	0.47	
90.0	3.23	0.41	0.61
100.0			0.25

Corrosion in mm/year; boiling point

	20% Formic Acid	40% Formic Acid
Type 317L	0.23	0.43
Alloy 2205 (S31803)	<0.025	
Alloy 255 (\$32550)	0.025	<0.025



Acetic acid

Acid	Test	Test Duration	Corrosion Rate (mm/	
Concentration (%)	Temperature (°C)	S30200 o S30400		\$31600
0 to glacial	Room	Up to 157 days	< 0.003	< 0.003
1	Boiling		< 0.003	<0.003
2.2 ^(A)	Boiling	45 days	>0.79	0.20
10	Boiling	5-7 days	1.78	0.008
20	Boiling	112 days	0.07	0.018
50	Boiling	4 days	3.30	<0.025
80-100	Boiling	80 hours	0.30	< 0.003
Glacial	Boiling	21 days	0.79	0.020

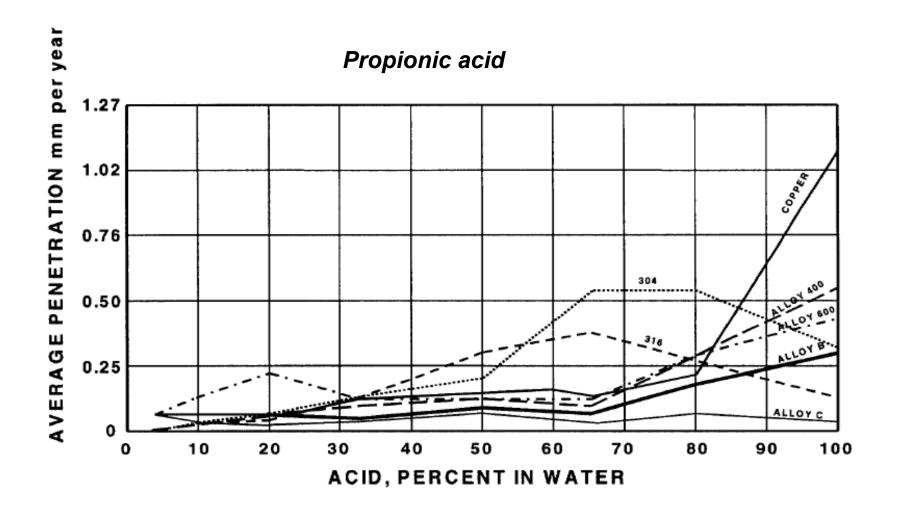


Mixed acid

Corrosion rate, mm/year 7472 0.25 S31603 50% acetic acid S31703 0.20 0.15 S32205 N08028 0.10 S32750 and N10276 0.05 no attack N06625 N06455 N06022 0 5 10 15 20 25 0 HCOOH, weight-%

Corrosion rate in 50% boiling acetic acid with different formic acid content







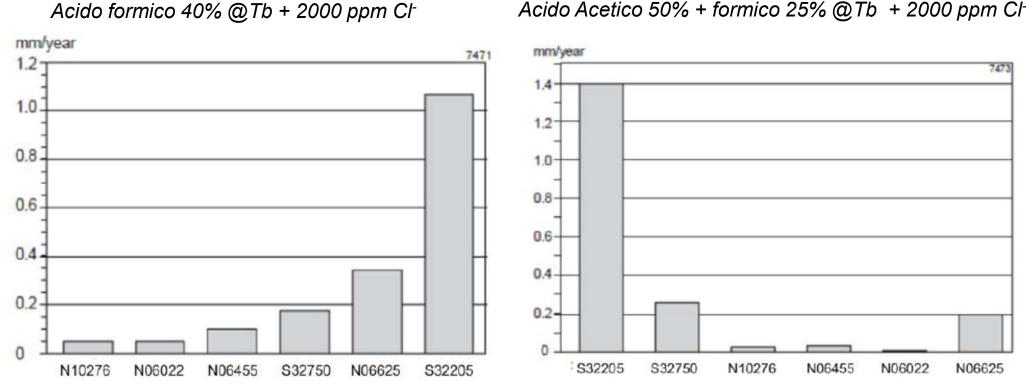
Presence of CO₂

If in the aqueous phase, in addition to the organic acidity, CO₂ is present, the traditional stainless steels are show no significant increase in the risk of corrosion.

Presence of chlorides

If **chlorides** (high in certain feedstock a RUCO) are present in the aqueous phase together with organic acidity, stainless steels are subject to even severe corrosion (**pitting and SCC**)

Ni-Cr-Mo alloys with high PRE (e.g. 625, C276) are more resistant



Acido Acetico 50% + formico 25% @Tb + 2000 ppm Cl⁻

Organic acid with NO water

- Process fluids characterized by high T conditions (T> 100 ° C) and absence of water, are corrosive to carbon steel in the presence of various types of organic acids.
- Similar to naphthenic acid corrosion in traditional refineries, which however is function of the sulfur content of the stream, turbulence, flow conditions, type and content of acids, and which is typically active for T> 200 ° C.
- However, even in traditional refineries corrosion issues by organic acids in anhydrous hydrocarbon fluids for lower T (about 150 ° C) as "low temperature naphthenic acids" are reported → organic acids with a lower molecular weight.

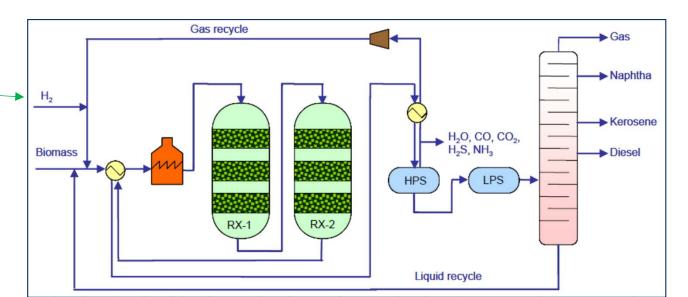
ORGANIC ACID TYPE		TAN	CORRO	CORROSION RATE, mm/year			
	ть °С	mg KOH/g	At T _b , °C	At 195°C	At 100°C		
Aliphatic Acids:							
Formic acid	102	599	12	-	11		
Acetic acid	114	634	21	-	20		
Propionic (propanoic) acid	141	788	23	-	18		
Butanoic (butyric) acid	164	629	46	-	27		
tert Butylacetic acid	181	471	33	-	6		
4-Pentenoic acid	183	550	61	-	6		
2-Ethylbutyric acid	186	480	40	-	17		
3-Pentenoic acid	190	538	34	-	8		
Hexanoic acid	200	476	99	-	2		
trans 2-Pentenoic acid	200	542	54	-	19		
Heptanoic acid	218	430	179	-	8		
Nonanoic acid	244	352	195	52	1		

CS corrosion rate in pure organic acid



Organic acid with NO water

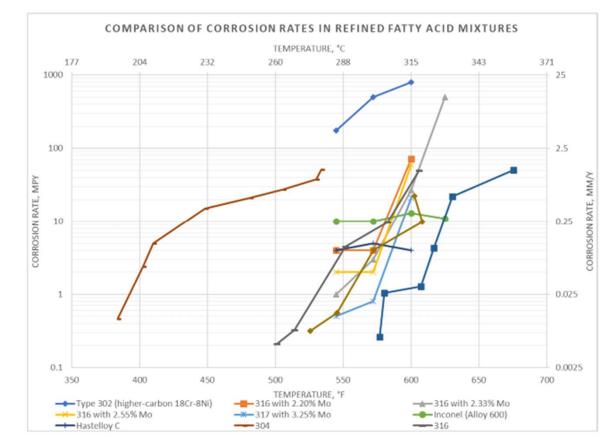
- In the presence of organic acids with no condensed water for T> 100 ° C (biofuels yet to be refined with a fair content of acids of various molecular weight), an alloy with an adequate Mo content must be used to limit high T corrosion:
- 317 825 625 C276
- In areas with high turbulence and potential high chloride content, it is advisable to choose alloys with a high Mo content (nickel alloys)
- As in fossil refinery, streams with H₂ and organic acid at high temperature are less corrosive from organic acid corrosion point of view
 - \succ H₂ tends to destroy organic acids
 - Standard 300 stainless can fit





Free Fatty Acid topic - FFA

- Bio-oils and biomass-oil contain greater quantity of FFA
- Triglycerides in bio-oils can convert to FFA during storage, pretreatment and feed circuit to reactor in hydrotreatment
- Corrosion can be similar to naphthenic acid corrosion
- High T corrosion T> 250 °C
- In H₂ free high T stream, **Mo containing SS or Ni-based alloys** resist better
- Downstream H_2 FFA corrosion is mitigate, but less corrosion data than traditional refining \rightarrow Mo free SS can Fit (For H_2/H_2S corrosion) -> experience needs to be gained



3

* Sutton, Kirkham - Converting Hydroprocessing Equipment to Produce Renewable Diesel from Soybean and Corn Oil: Corrosion and Materials Considerations



Effluent systems

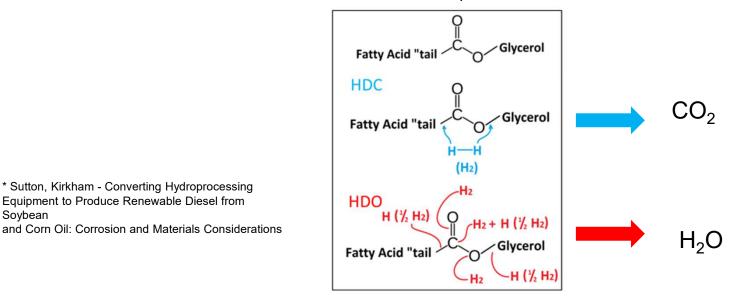
- Effluent from reactor (hydrotreating) processing pure bio-oils and biomass-oil ٠ contains high content
 - CO₂ from HDC reactions
 - H₂O from HDO reactions

* Sutton, Kirkham - Converting Hydroprocessing

Equipment to Produce Renewable Diesel from

Soybean

- CO₂ corrosion on CS in effluent systems (low pH) ٠
- **Feedstock rich in chlorides (**organic and inorganic) produce HCl in effluent (high ۲ risk of corrosion in CS and traditional SS \rightarrow Mo containing Ni-alloys needed (injection of neutralizer?)
- **Mixed feedstock (petroleum + bio)** induce the presence of $NH_3 \rightarrow$ buffering ٠ effect pH in effluent but increases risk of NH₄CI deposition and corrosion





Conclusions

- The transport, storage (raw materials and finished products), production and combustion phases of biofuels/renewable fuels could present **different** corrosion problems than fossil fuels.
- The presence of greater quantities of **oxygenated species**, **water and organic acids (also FFA)** entails variable risks of corrosion.
- CO₂ and chlorides may also be present which dissolve in the aqueous phase ("low T" corrosion)
 - CO₂ corrosion requires SS
 - Process fluids with organic acids in the aqueous phase require SS with Mo (e.g. 316, 317, 2205)
 - If chlorides + organic acid are present → Ni-Cr-Mo alloys (e.g. alloy 625 or, in aggressive conditions, C276)
- In anhydrous streams with organic acids at T> 100 ° C corrosion problems due to "high T" are triggered (similar to NAP Acid): need to use steels with high Mo type 317 825, 625
- Hydrogen mixing mitigate corrosion at high T (lowering the TAN) \rightarrow standard 300 SS cab fit, but less data than petroleum refining unit!



Appendix 8

Integrated real-time corrosion prediction as a path for corrosion digital twin approach

(Slawomir Kus)



EFC Working Party 15 "Corrosion Refinery and Petrochemistry Industry" Spring Meeting - 24th March 2022

Integrated real-time corrosion prediction as a path for corrosion digital twin approach

Dr Slawomir Kus Lead Corrosion Consultant Honeywell Connected Plant, Bracknell, UK



Agenda

- Digital Transformation quick recap
- Corrosion & Digital Transformation where are we now?
- Software Sensor & Corrosion Digital Twins integrated approach for corrosion management
- CDT/corrosion software sensor
 - Integration with other corrosion analytical/assessment tools
 - IT Security
 - Challenges
- Summary

Digital Transformation - recap

• **Digitization:** encoding of analog information into a digital format

 Digitalization describes how IT or digital technologies can be used to alter existing business processes

• **Digital transformation** is the process of using digital technologies to create new / modify existing business processes, culture, and user experiences that helps to create and appropriate additional value for the company. ⁽¹⁻³⁾

When we do : it the bottle

imply the index of B do

Wireless corrosion transmitters

Digitization

Gateway

DCS/Historian

People

Customer

Strategy

Digital

Transformation

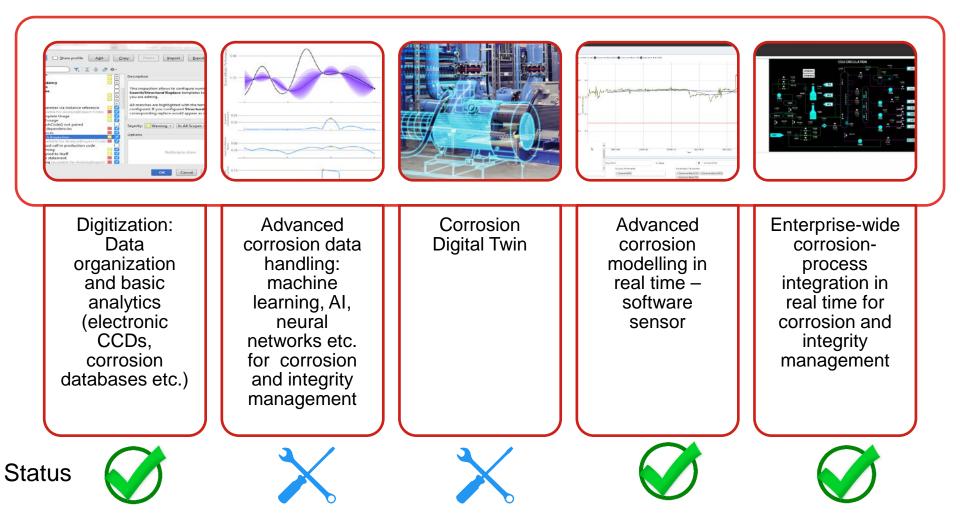
Technology

Organization

Culture

Operator's panel

How Digital Transformation is Progressing in Corrosion World



* After Glaessgen, Edward, and David Stargel, Editor, 2012. The digital twin paradigm for future NASA and US Air Forseyebiotemfidential - @2022 by Honeywell International Inc. All rights reserved.

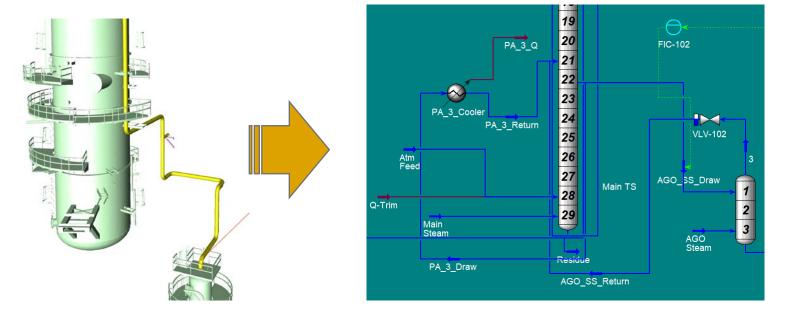
Digital Twin (DT)

* A Digital Twin is an integrated Multiphysics, multiscale, probabilistic simulation of a complex product that uses the best available physical model, real-time sensor data, historical data etc. to mirror the life of its corresponding twin.

Creation of DT for technological process is virtually "easy"

- large number of process controllers
- "live" and past data available in process Historian

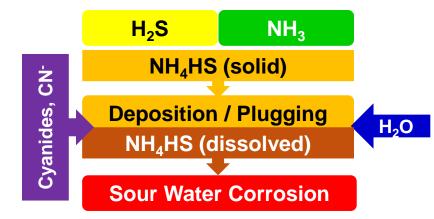
- reliable thermodynamic/kinetic models
- usually modelling physical processes not involving complex chemical reactions



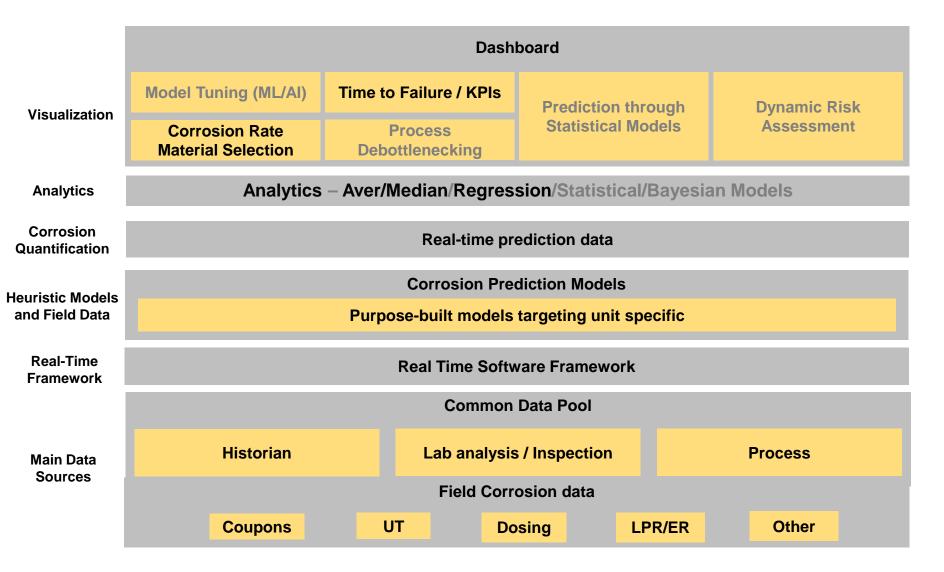
Corrosion Digital Twin (CDT)

- Development of CDT is complex.
- Corrosion data flow is "lean"
 - Very few hardware corrosion monitoring points
 - Hardware locations are based on historical data and accessibility
 - Installation and expansion of hardware corrosion monitoring is a costly and time consuming effort
- Real-time, online, corrosion data streams are rarely linked with "live" process data:
 - data interpretation is complex
- Digital Transformation" in corrosion monitoring & management requires accurate corrosion prediction



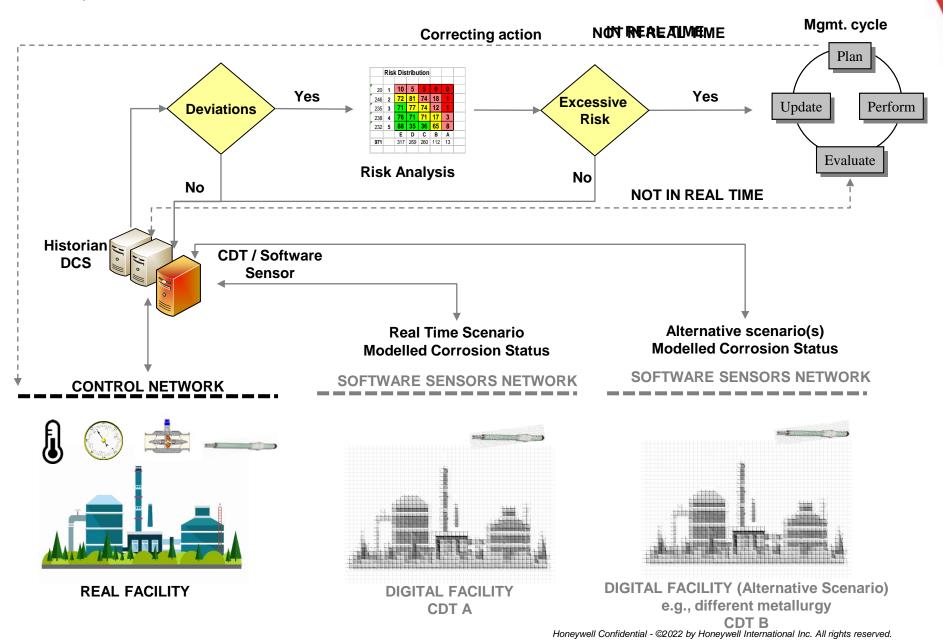


Software sensor / CDT Architecture

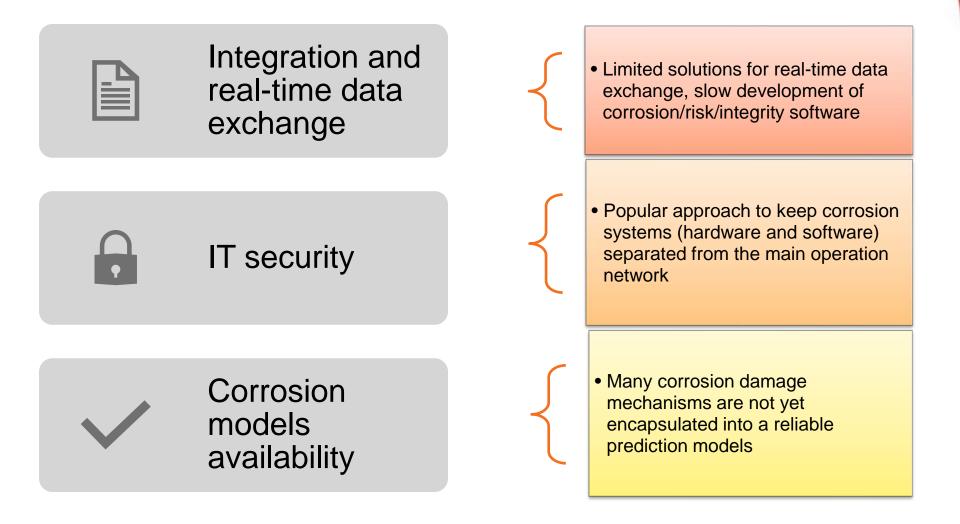


Integrated CDT approach

Example

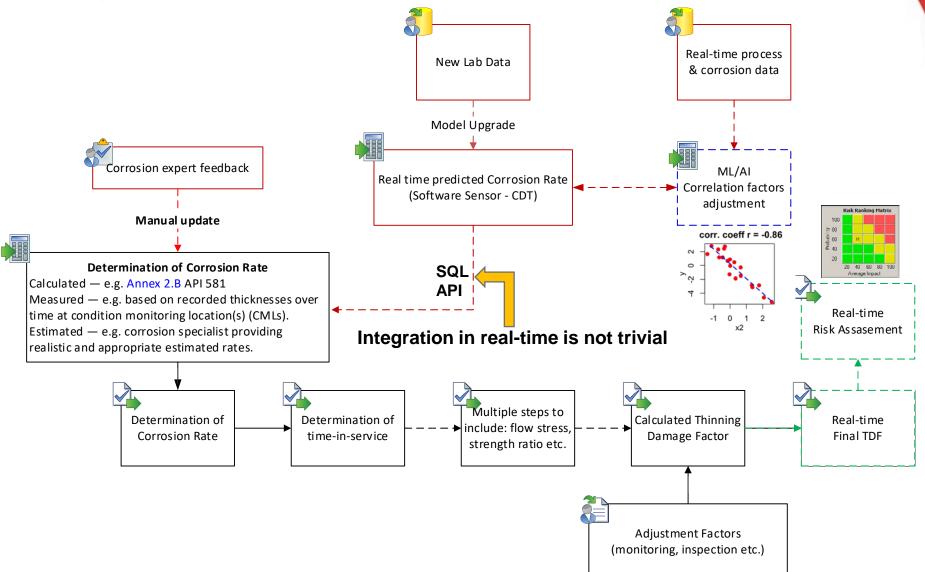


Software Sensor/CDT – Challenges



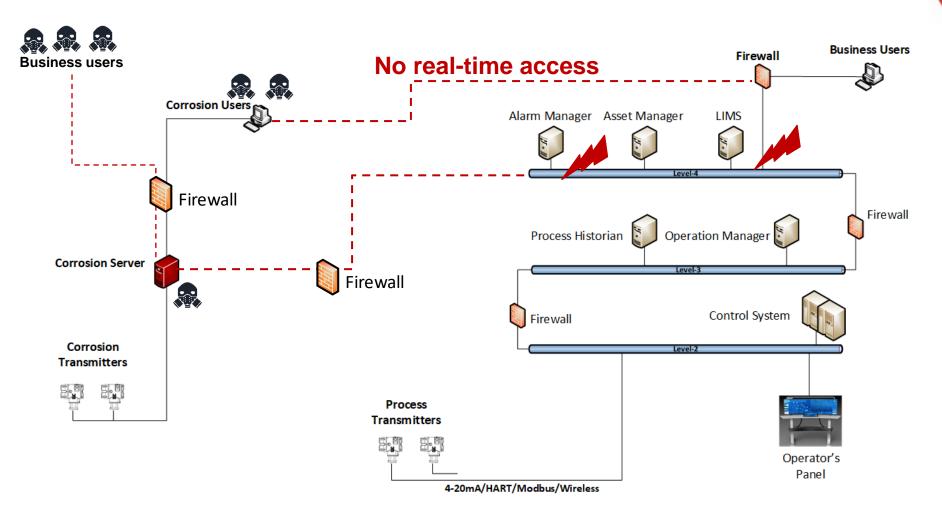
CDT/Software sensor framework and RBI process

simplified example of work flow



12

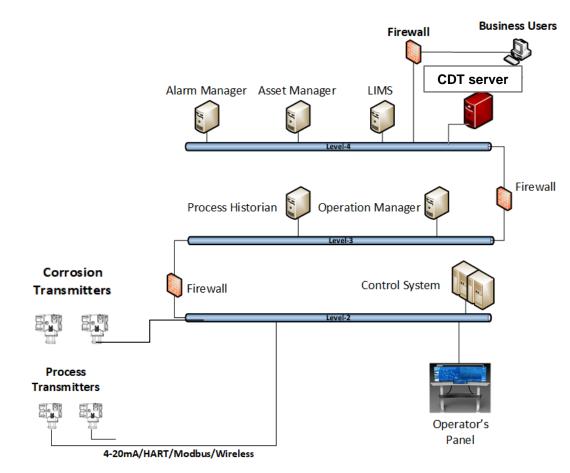
CMS IT security – traditional approach Example



Separate "Corrosion Server"

Typical Plant's Network System

Real time CDT/software sensor – IT security

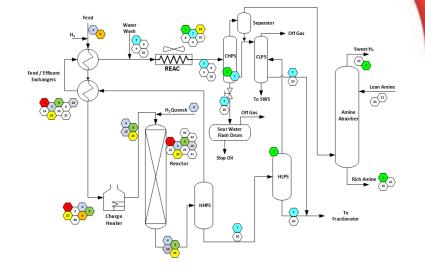


Benefits:

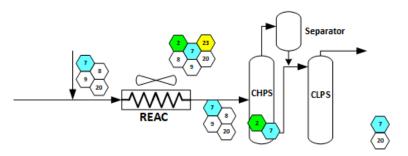
- Software sensors server is connected in real-time with all corrosion-process data streams
- No external interaction (bad actors) with RT server
- IT has full control on configuration and corrosion data streams

CORROSION MODELS AVAILABILITY

- API RP 571 2020 distinguishes of 67 various damage mechanisms present in the refining industry.
- There are <10 of well-developed and established corrosion models.



- Need to focus on "active" DMs
 - NH4HS corrosion (7)
- Progress in application of ML and AI will enhance/expand existing models capabilities and build new
 - Erosion-corrosion (20) 🗙
- New models development (lab researches)
 - NH4Cl corrosion (8) 🗙
 - HCI corrosion (9)



Summary

- Digital Twin is a key element of plant digital transformation
- Corrosion "Software Sensor" framework aka Corrosion Digital Twin (CDT) allows for real time integration of process and corrosion data.
- CDT allows for duplication of number of corrosion processes and predict their current and future status
- CDT enables enterprise-wide access for corrosion information while operating within safe and secure IT oversight.
- Development on real-time integration of CDT and risk assessment tools is required.

Appendix 9

Emerson automation solutions: digital connected services enhance value of corrosion monitoring data

(Kjell Wold)

"Digital Connected Services Enhance Value of Corrosion Monitoring Data "

EMERSON

Presenter: Kjell Wold, Emerson Corrosion and Erosion

Emerson Confidential

Corrosion Measurement Numbers Depend on Many Parameters

Why isn't my monitoring system providing the info I need for my corrosion management?



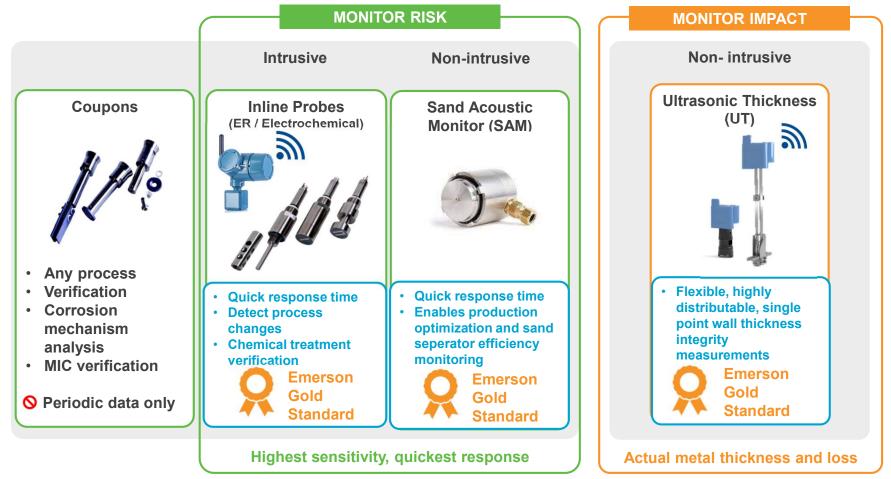
Suitable (combination of) corrosion technologies for the application?

System performance and uptime?

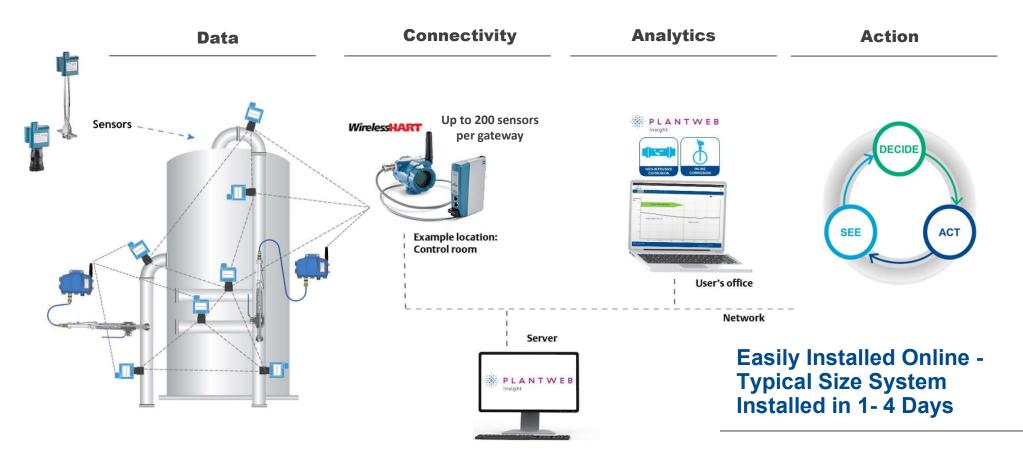
Access to and understanding monitoring data?

Data converted to actionable information?

Your Corrosion and Erosion Challenges Require a Complete Sensing Portfolio



Continuous, Real Time Corrosion Risk and Asset Health Data Directly to Desk



Corrosion and Erosion Remote Digital Services – Site Visits not Required

Remote Health Check

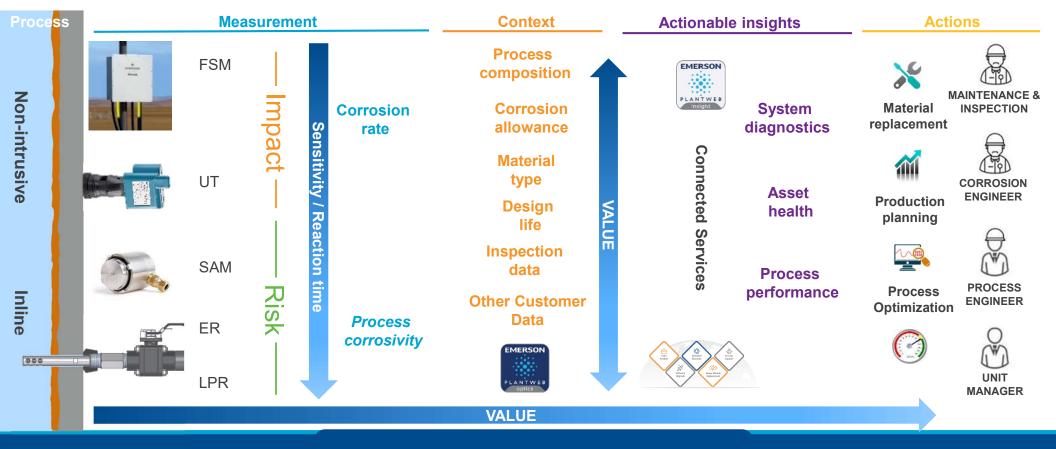
- VPN Remote Acess
- Screen Sharing Sessions
- Off-line Data Base Back-up Analyses
- Value
 - Cost effective confirmation on system performance
 - Custom built system improvement increases uptime

Data Base Services

- Merging or splitting of data bases
- Migration of historic data from Permasense Data Manager to Plantweb Insight Corrosion Application
- Value
 - Cost efficient database management
 - Focus on priority information



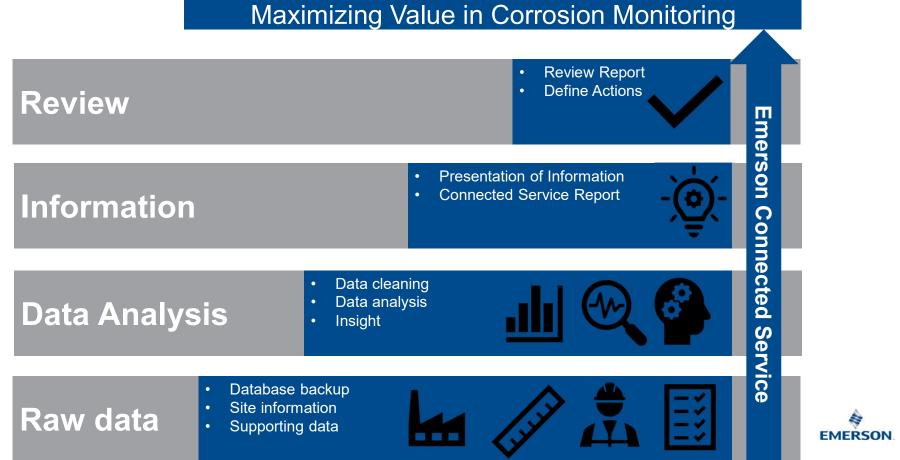
Emerson Confidential



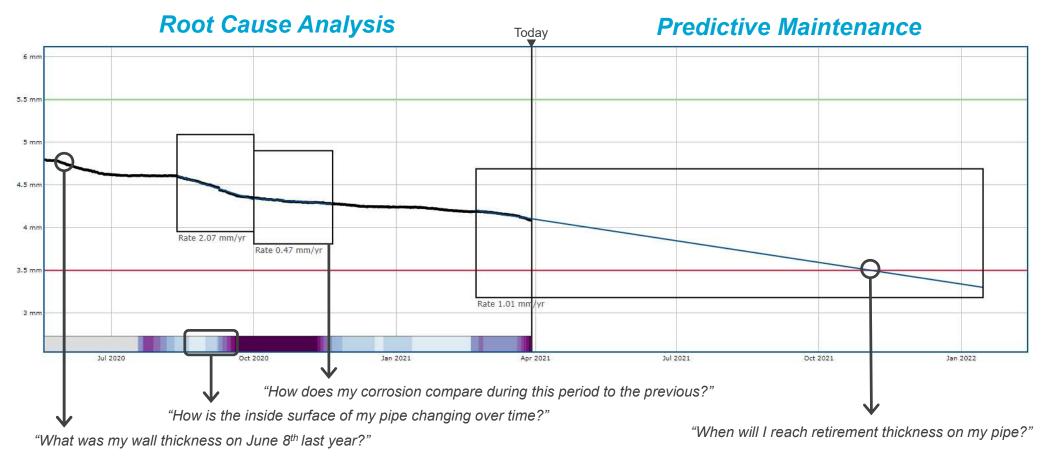
Connected Services Turns Data into Actionable Information

Unlock True Value of Corrosion Monitoring System

Remote Data Enhancement - Data Analysis Delivering Information

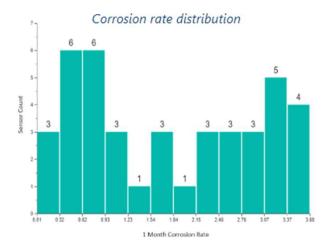


Thickness Monitoring Data for Root Cause Analysis of Corrosion Events and Turnaround Scope and Timing Improvement

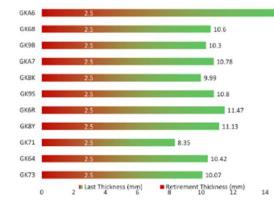


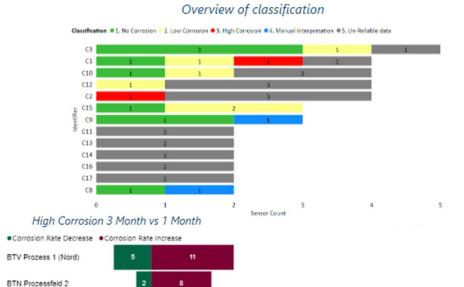
Dashboard to Gives Accessible Overview of Corrosion Activity

14.88



Last thickness vs Retirement thickness





System Summary w/ Maintenance Breakdown

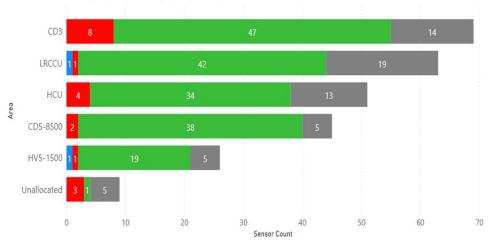
BTN Prozessfeld 1



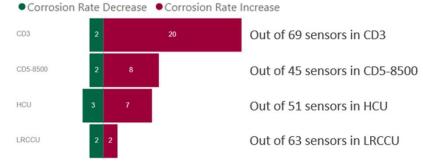
Sample Corrosion dashboard

Histogram of Corrosion Rate Distribution ¹⁸⁰ 7 168 160 -140 -120 -100 -80 -60 -40 -20-1 0 0 0 0 0 0 0 0 0 0.00 0.05 0.10 0.15 0.20 0.25 0.31 0.36 0.41 0.46 0.51 0.56 0.61 0.66 0.71 0.76 0.82 0.87 0.92 0.97 1.02 1.07 3 Months Corrosion Rate (mm/yr)





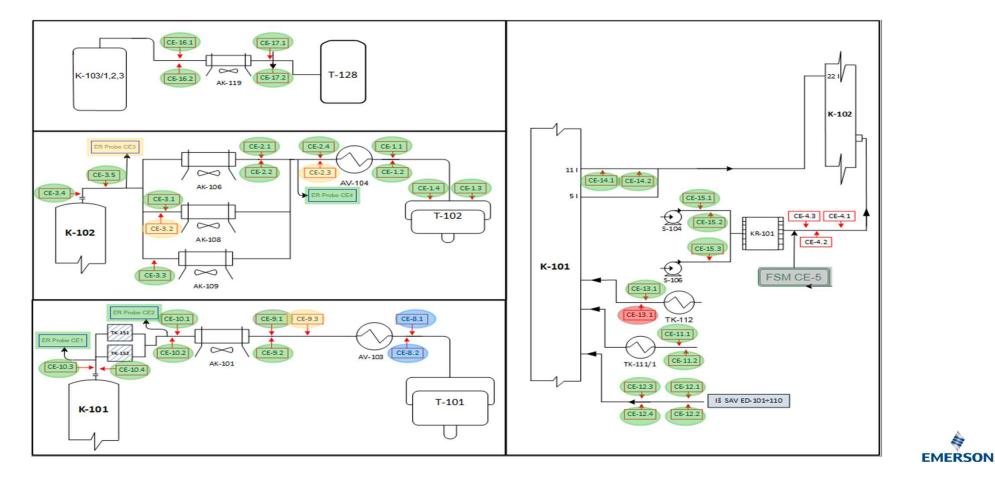
Corrosion Rate Variation (1 Months vs 3 Month)



If the difference between 1 Month corrosion rate and 3 Months corrosion rate is (above/equal) \geq 0.05mm/yr then the sensor will be classified as Corrosion Rate Increase. If corrosion rate difference is (below/equal) \leq -0.05mm/yr, then the sensor will be classified as Corrosion Rate Decrease.



System Summary – This Quarter



Summary

- Wireless standardization and digital data has made on-line communication affordable and allows remote handling of housekeeping information as well as corrosion data
- Remote Digital services contribute to proactive maintenance and trouble shooting with a minimized need for site visits

 Data analysis and reporting by external experts ensure correct data interpretation and that information is converted to actionable information

Appendix 10

Lowering the top temperature in FCC fractionator: corrosion issues

(Marco de Marco)

Lowering the Top Temperature in FCC Fractionation Tower : Corrosion Issues

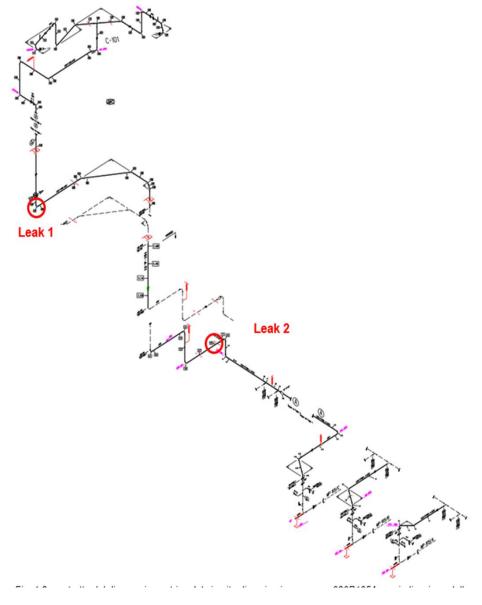
M. De Marco - IIS



Introduction

- FCC Unit Fractionation Tower
- Top Pump Around (TPA) line from column to pumps
- N° 2 leaks in 2021
- 30 yr old plant (1982)
- Revamping of the TPA circuit in 2015.
- New line installed in 2015
- No temperature probe in TPA after 2015
- Data only on T overhead
 - Lower than before revamping

•	Ts:	not measured
•	Ps:	0.6 barg
•	Fluid:	Top Pump Around
•	Diam.:	12"
•	Thickness:	8,38 mm
•	CA:	3,00 mm
•	Material:	ASTM A106 Gr. B.

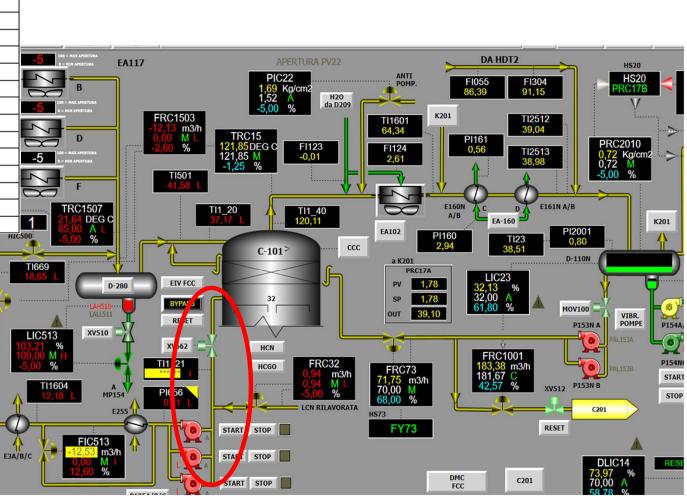




Introduction

• Overhead T controlled to optimize naphta cut in TPA

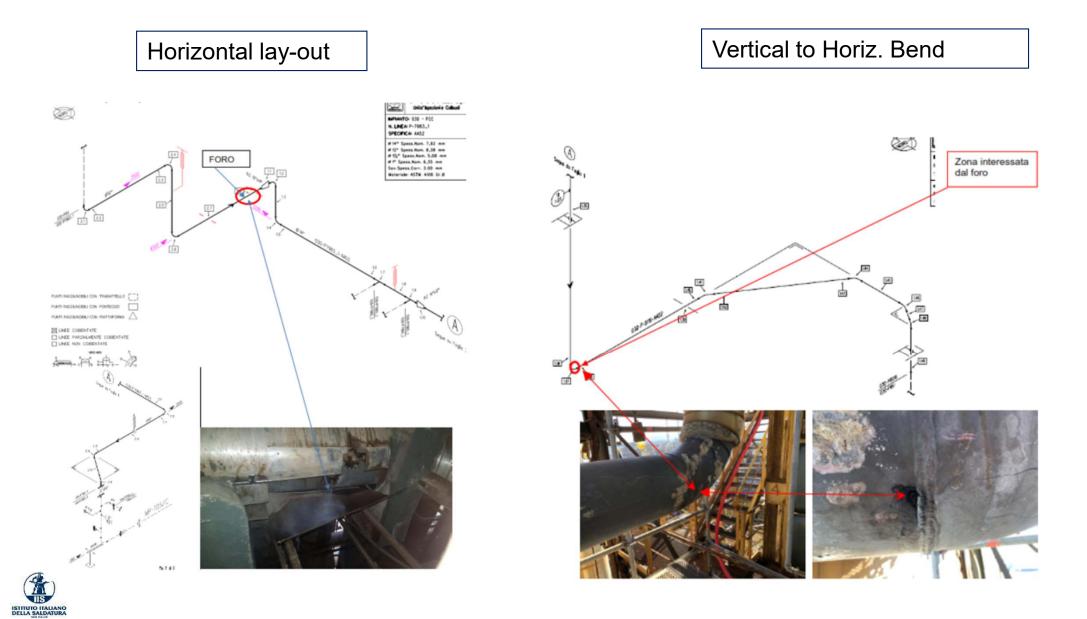
PARAMETER		VALUE	
DENSITY A 15 °C(DEN00)	kg/m3	736]
T.V.R.(TVR00)	HPA	625]
COLOUR SAYBOLT(COS01)	*	15	
C4 TOTALS(NC400)	VOL%		
I.B.P.(H0100)	C°	31	-5
5% REC.(H0200)	C°	44	
10% REC.(H0300)	C°	49	
20% REC.(H0400)	C°	57	-5
50% REC.(H0700)	C°	91	4
90% REC.(H1100)	C°	158	
95% REC.(H1200)	C°	168	-5
F.B.P.(H1300)	C°	181	5
EVAP. A 70 °C(H1400)	VOL%	34,1	
EVAP. A 100 °C(H1500)	VOL%	55,6	
EVAP. A 150 °C(H1600)	VOL%	85,2	1





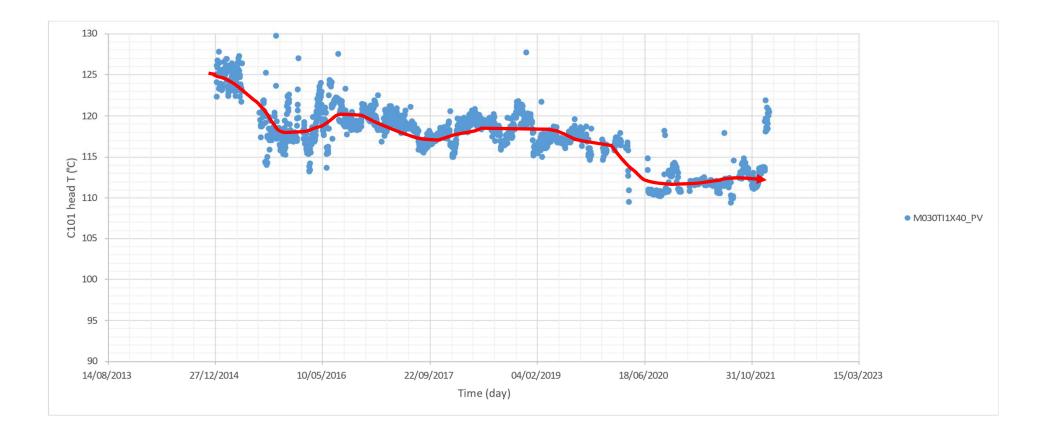
LEAKS

- N°2 leak event for internal corrosion
- Diffused internal metal loss in the line revealed by NDT



Overhead T trend

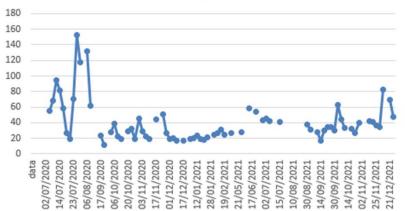
• Overhead temperature was progressively reduced over time

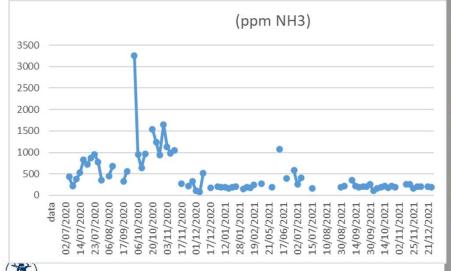




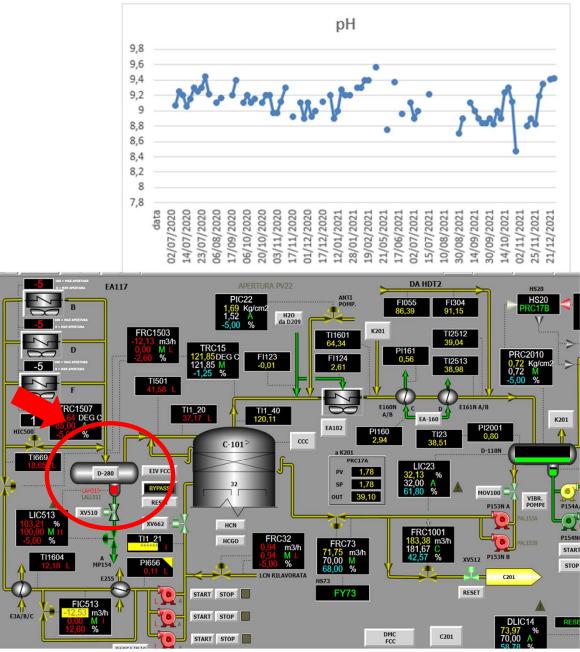
Overhead T trend

Process KPI data
 Downstream accumulator – low T
 Chlorides (ppm NaCl)





ISTITUTO ITALIAN DELLA SALDATU



DAMAGE – LEAK 1

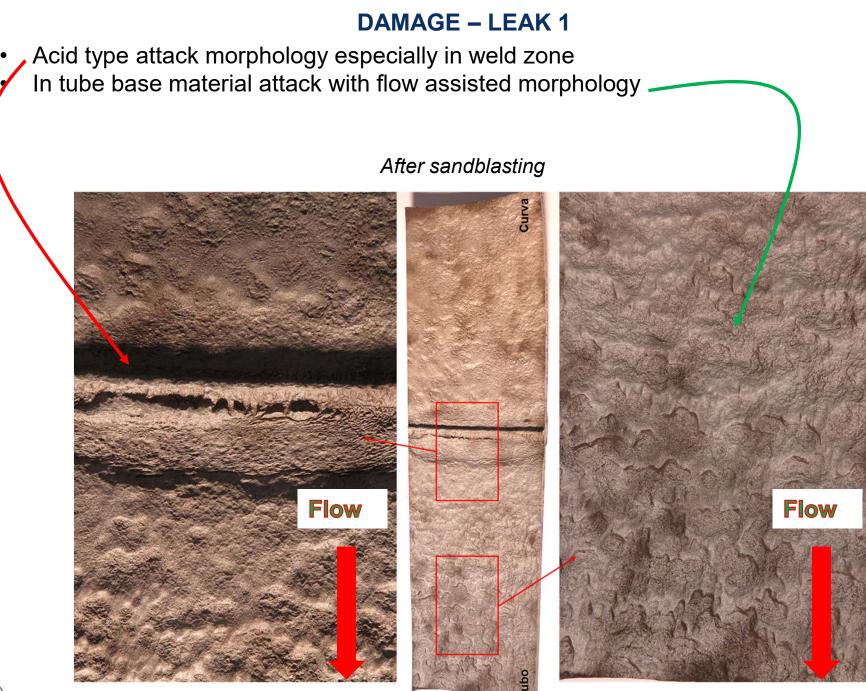
- Internal corrosion
- Bend and horizontal portion of tube downstream of bend
- Weld area (HAZ) with high corrosion rates
- Black and brown deposits





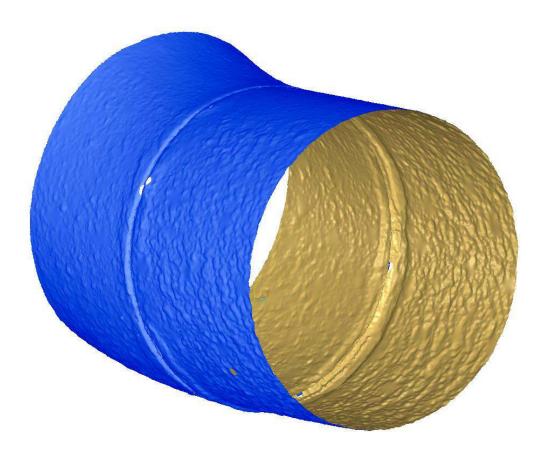


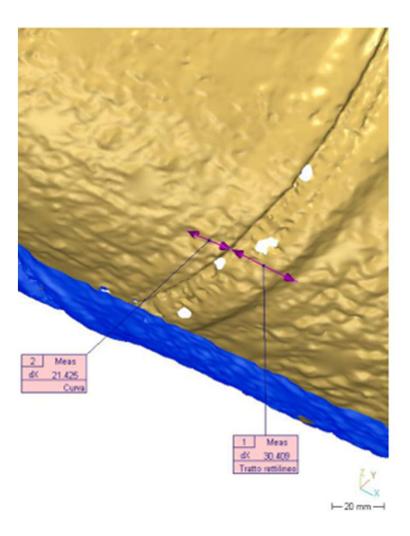






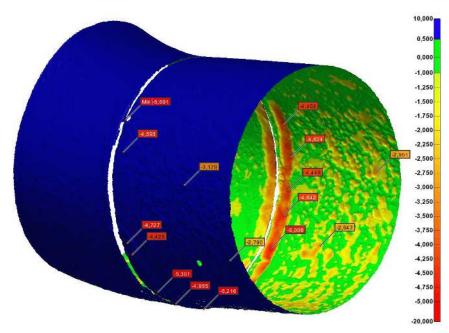
Corrosion mapping

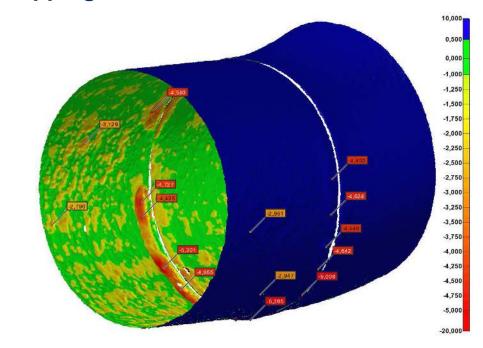


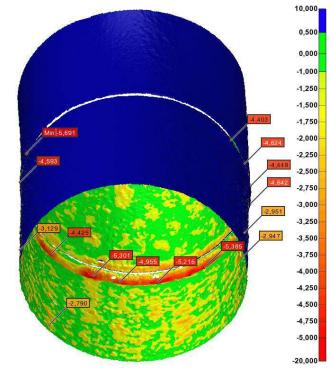




Corrosion mapping

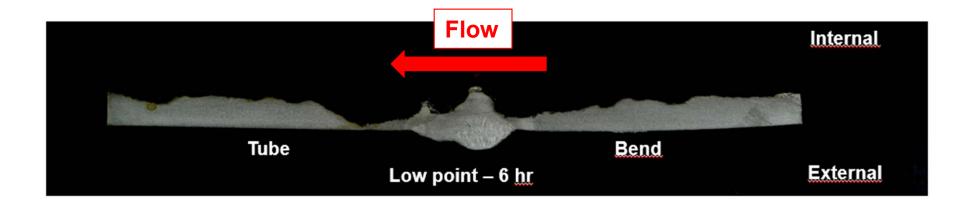


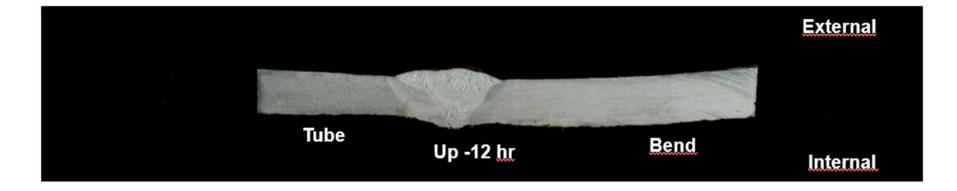






Corrosion morphology

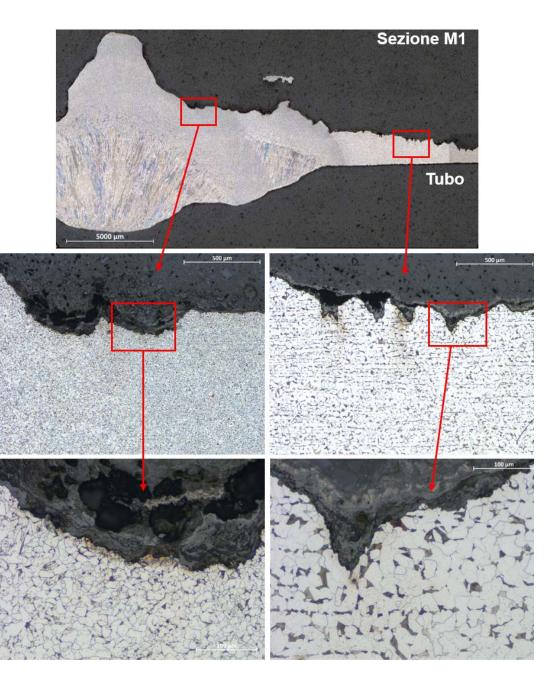






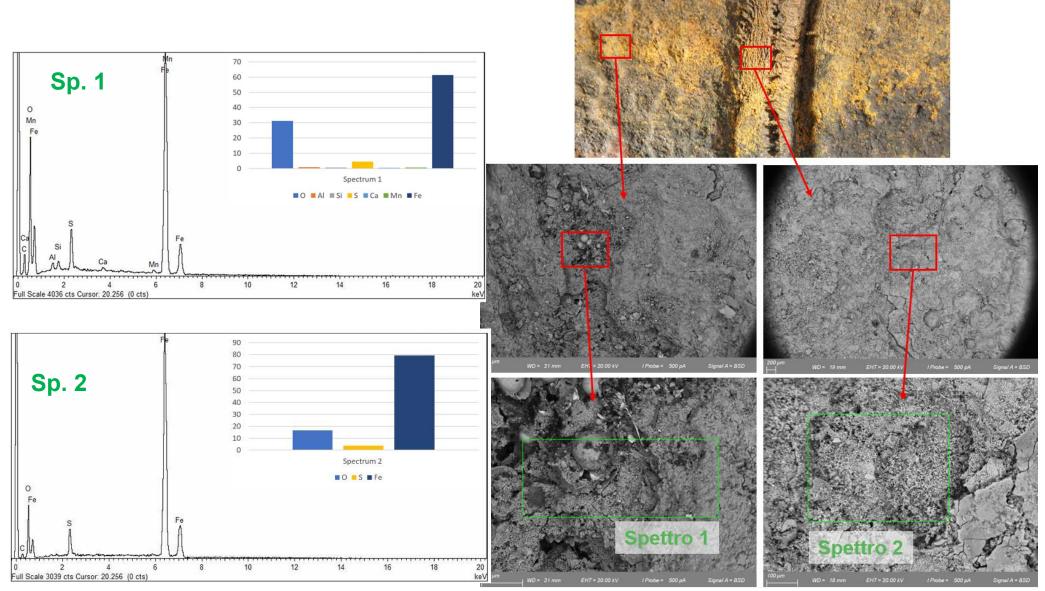
Corrosion morphology

Micrographic examination

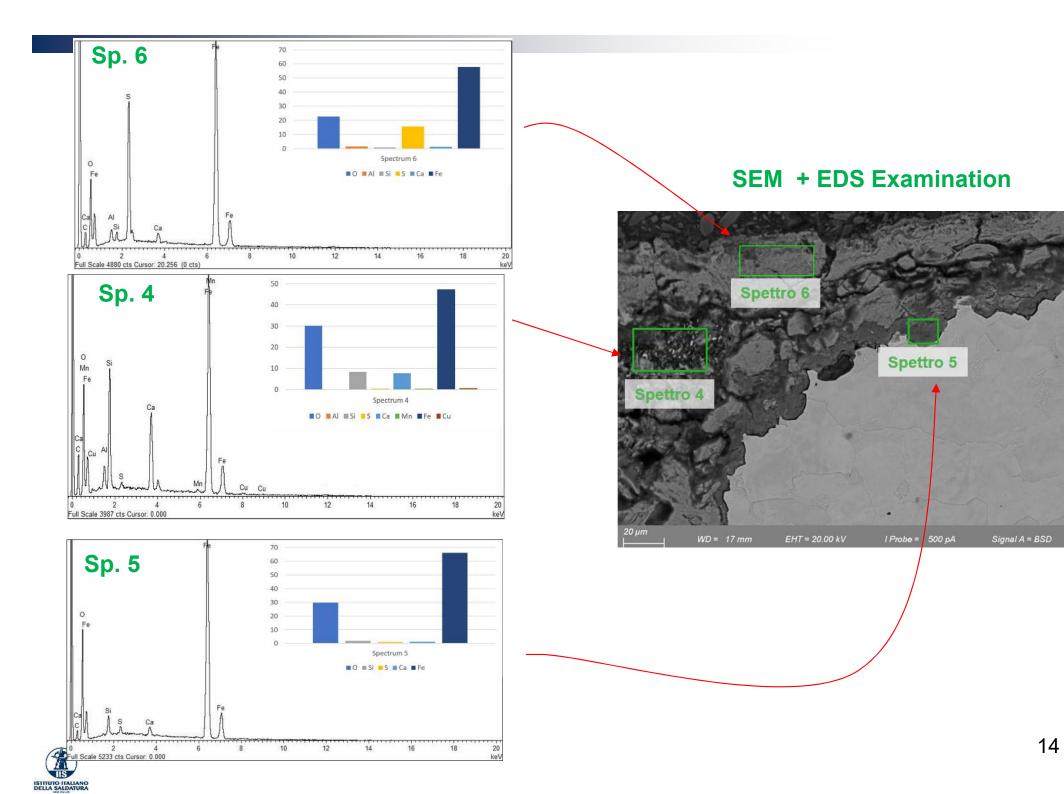




SEM + EDS Examination

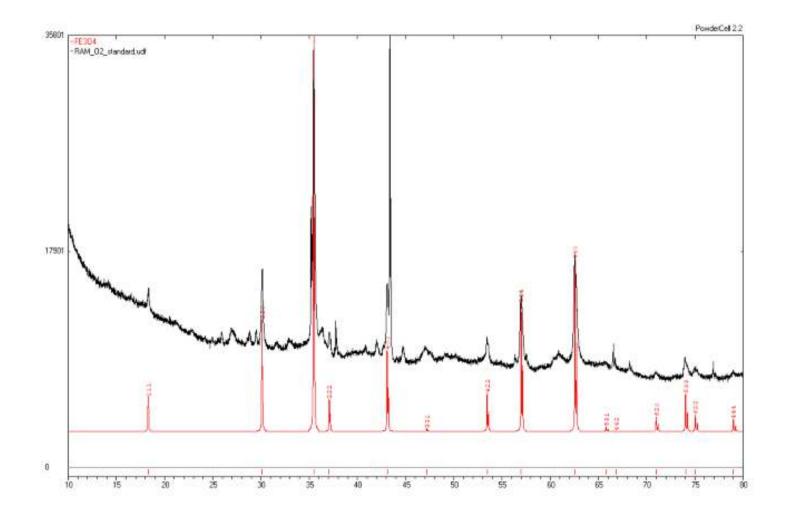






XRD

- Permits to characterize the crystalline part of deposits
- $Fe_3O_4 \rightarrow no oxygen in the environment (as expected)$





Water Extract

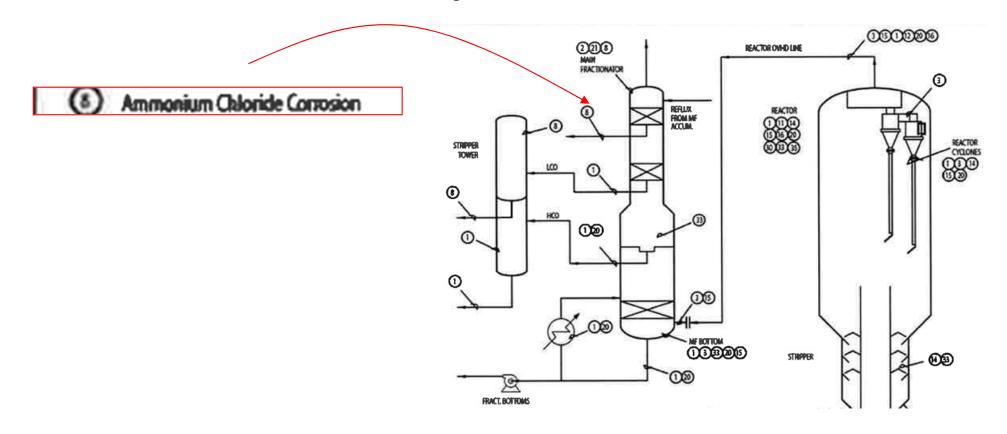
- No acidic
- Low chlorides

Parameter	Risultato
Aspect	solid
Color	Brown
Odor	No odor
State	Powder solid
pH (upH)	8,23
Chlorides (mg/kg)	130
Fluorides (mg/kg)	217
Phosphates (mg/kg)	< 100
Sulfates (mg/kg)	638
Nitrates (mg/kg)	< 100
Nitrites (mg/kg)	< 100
Soluble Ammonium (mg/kg)	314
Calcium (mg/kg)	525
Magnesium (mg/kg)	38,5
Potassium (mg/kg)	430
Sodium (mg/kg)	89,9



Discussion

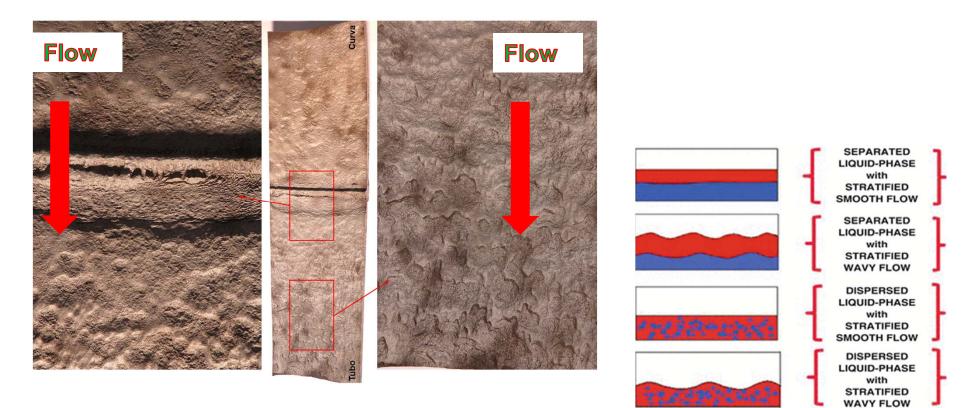
- Corrosion due to condensed water phase.
- High quantity of water withdrawn in TPA
- Overhead temperature progressively low in last months \rightarrow increases water cut in TPA streams
- Typically, in FCC Unit TPA corrosion associated to NH₄Cl corrosion → under-deposits acid corrosion in case of low water cut → high water cut washes salts





Discussion

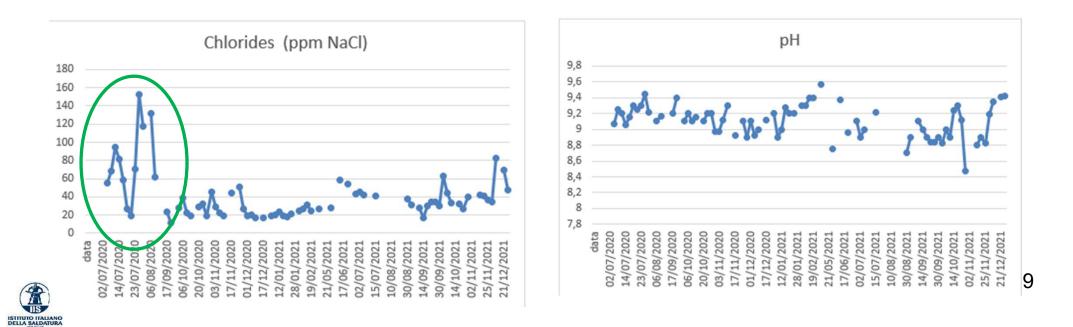
- Morphology more associated to acidic water phase (stratified flow) and flow assisted corrosion.
 - Weld metal not affected (More noble?)
 - HAZ most affected (electrochemical or flow effects?)
 - Deposits not acidic , no detectable chlorides in deposits





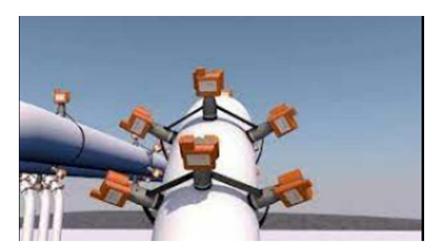
Discussion

- Water analyzed in **downstream accumulator** (low T and total condensate)
 - Spikes in chlorides in 2020 (until sept. 2020).
 - pH between 8,5 and 9,6 (slightly alkaline) buffering effects of NH₃ at low T
 - Unknown pH in first water condensate (line of interest) at T> 100 °C (ammonia in vapor / chlorides in condensed phase) - No simulation carried out
 - No data 2015 2020 (?)
 - Periodic ingress of (organic/inorganic) chlorides in the UNIT?
 - Other acids in feed to fractionator (e.g. SOX, organic acids)???

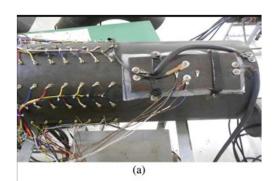


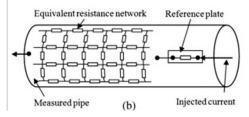
Discussion – Corrosion management

- Until Now \rightarrow
- Washing waters in overhead circuit with corrosion inhibitors (filming/neutralizing amine).
- In TPA only dispersant
- Opportunity \rightarrow
- Use Neutralizer in TPA? (risk of fouling?; accumulator boot water is already Alkaline in nature → how control injection?)
- Process simulation (dew point, salting point?)
- Application of UT Probe or FSM systems for real-time thickness monitoring and associate them to process variables
- Water withdrawal in column (dedicated water draw tray)











Appendix 11

A Hybrid Approach to Volatile Corrosion Inhibitors (VCIs) and Soluble Corrosion Inhibitors (SCI) for addressing CUI/Scab Repair and Flange Corrosion

(Dale Matthews)





Zerust ZIF Tape

EFC WP15 "Corrosion in refinery and petrochemistry"

A Hybrid Approach to Volatile Corrosion Inhibitors (VCIs) and Soluble Corrosion Inhibitors (SCI) for addressing CUI/Scab Repair and Flange Corrosion.



- 1. What are VCI's and how do they work.
- 2. CUI Prevention, Scab repairs using ZIF Tape (Zerust Inhibitor Fusion Tape)
- 3. ISO 19277



What are VCl's?

And how do they work?



How Vapor Corrosion Inhibitors (VCIs) Work

How do VCIs work?

1 - The molecules will form a molecular film on any metal they encounter. This film prevents oxygen from reaching the base metal and therefore the corrosive reaction.

2 - The VCI and SCI will neutralize the PH of particularly acidic environments, raising the pH to a level of 8/9 which results in a dramatic reduction in corrosion rates)

3 - The VCI and SCI will search out and neutralize any contaminants found in the area in which they are introduced. Such as acidic and ionic species, sulphides and chlorides.



ZIF Tape – CUI/Scab Repairs/Flanges





What is ZIF Tape...

- 1. ZIF tape is a self fusing, corrosion inhibiting tape based on silicone elastomers with proprietary Zerust corrosion Inhibitor chemistry impregnated into the matrix.
- 2. ZIF is cold applied and requires only an ST2 surface prep Wire Brush and Wipe
- 3. Strong mechanical properties/robust due to silicone nature. 10 years +
- 4. Only bonds to itself, resulting in a very easy removal and easy inspection process.
- 5. No residues following removal.
- 6. Translucent allowing visual inspections.
- 7. UV stable.
- 8. Minimizes entire work parties and entire processes resulting in large cost savings. Explain Inspections/Maximo processes...
- 9. Wide temperature range -40deg.C to +220deg.C
- 10. Tested to ISO 19277

Areas...

- 1. Valves/Flanges
- 2. CUI
- 3. Scab repairs
- 4. Coating defects





Winner of the French Oil & Gas Council Innovation Award for Zerust's® ZIF Tape

Valves





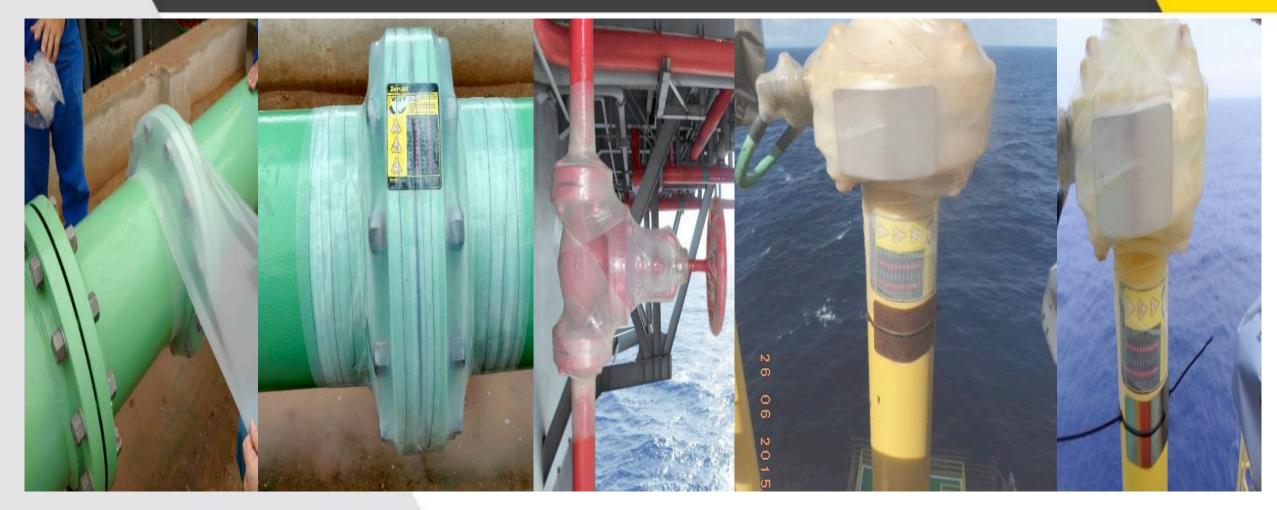


Edges Tied in with 2" ZIF Tape



Sticker indicating application date applied





CUI IS A MAJOR ISSUE ON INDUSTRIAL PIPING AMOUNTING TO APPROXIMATELY 10% OF PLANT'S MAINTENANCE COSTS – DEVELOPMENT OF PREVENTIVE ACTIONS HAVE BEEN NEGLECTED

Corrosion Under Insulation (CUI)

Description & Challenge

- CUI is a severe form of localized, external corrosion that mostly occurs on carbon, low alloy steel and stainless-steel which are insulated
- CUI is most prevalent in the chemical/petrochemical, refining, offshore, and marine/maritime industries. If left undetected, CUI can result in catastrophic leaks or explosions, equipment failure, prolonged downtime due to repair or replacement, and safety and environmental concerns
- CUI accounting for an estimated 10% of a plant's overall maintenance costs and 40%- 60% of its pipeline maintenance costs
- More than 90% of maintenance work related to corrosion detection based on risk-based assessment shows no corrosion and, therefore, could be avoided







Customer Potentials



Reduction of "unnecessary" maintenance costs



Revenue lost due to **unplanned down time** (opportunity costs)



Mitigation of accident potential: Direct accident costs & reputation costs

The global cost of corrosion is estimated to be US\$2.5 trillion, which is equivalent to 3.4% of the global Gross Domestic Product (2013)

CUI+ SCAB Repairs ...

12 month live refinery lines Antwerp 90 -120c





CUI+ SCAB Repairs ...

6 Months Jetty Side Antwerp

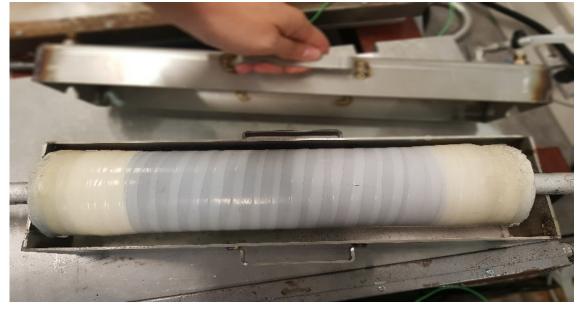


TESTED to ISO 19277 MULTI-PHASE CUI CYCLIC CORROSION TEST CUI-3 ...

The Tape was evaluated at a third-party (Element Testing NL) lab per the test cycle in ISO 19277 MULTI-PHASE CUI CYCLIC CORROSION TEST CUI-3. A brief outline of the test procedure can be found below:

Multi-phase CUI cyclic corrosion test CUI-3 A multi phase corrosion under insulation corrosion test according to modified ISO 19277 was conducted for 6 weeks...

- Test "coupon" is a bare steel cylinder
- Cylinder is internally heated by circulating oil at 175° C
- Cylinder wrapped with Tape and placed into test chamber
- Test chamber held for four hours at 175°C
- Test chamber filled with 5% NaCl solution and held at 175° C for four hours
- Test chamber drained and held at 175° C for four hours
- Test chamber filled with DI water and held for 4 hours at 175°C
- Cycle repeats for five days
- Test chamber opened, drained, cleaned and allowed to stand at ambient for two days



- Entire seven-day cycle repeated six times for a total test time of 1008 hours 15 cycles in total for a 6 week period.
- At the end of the test, the sample is evaluated for any defects in the Tape, in which apart from some discoloring, no defects were found.

Ease of Removal

No residue, glues or adhesives to remove



Inspection Cycles/RBI – ZIF – Part of the remedial tool kit.

Inspection – A Useful Tool

By minimizing the blasting element, entire work order/processes can be eliminated, such as: reducing hot work down to cold work permits, eliminating blasting on live lines (BOLL), reducing hazards and costs, eliminating heavy equipment such as blasting equipment, hoses, gauntlets, air purification tests, compressors, generators and so on.

Thereby, also eradicating coating equipment. Inspectors can use the Tape to a great effect during integrity inspections works and complete repairs following an NDT inspection.

This could drastically reduce workflows: reporting and entire work party management flows and saving multiple crews visiting the same jobsite to perform remedial works.



Zerust® Inhibitor Fusion (ZIF) Tape Conclusion

- Easy to Implement
- Substantial overall commercial savings vs. conventional coating systems.
- Non-Intrusive
- Continued In-Service Operational activities
- 5-10+ years of protection
- Ease to Inspect due to translucent nature of the ZIF Tape and ease of removal and/or reinstallation is required.
- Provides a 2 layer barrier: By means of a physical barrier of a robust Silicone based material and by means of a corrosion inhibitor that will form a molecular layer of protection and neutralize any contaminants.

THANK YOU!

Any questions? dale@rig-techsolutions.com

Appendix 12

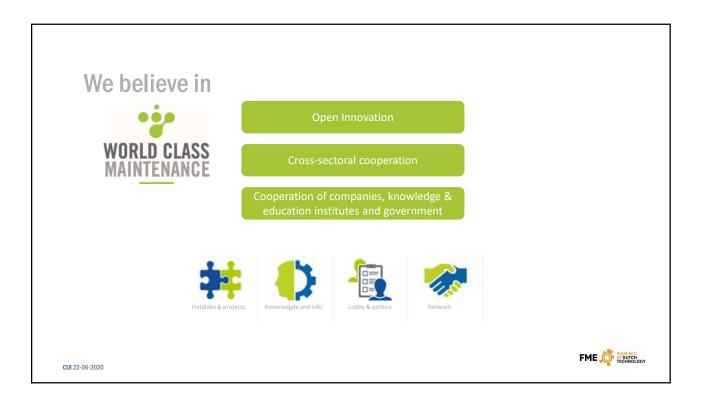
VCM best practice for Risk Based CUI management

(Geert Henk Wijnants)



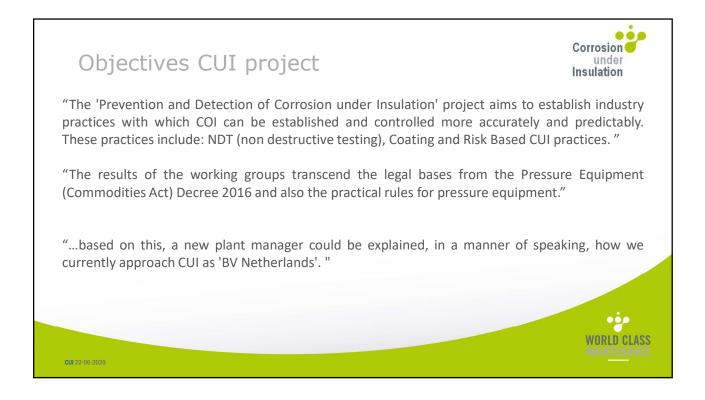






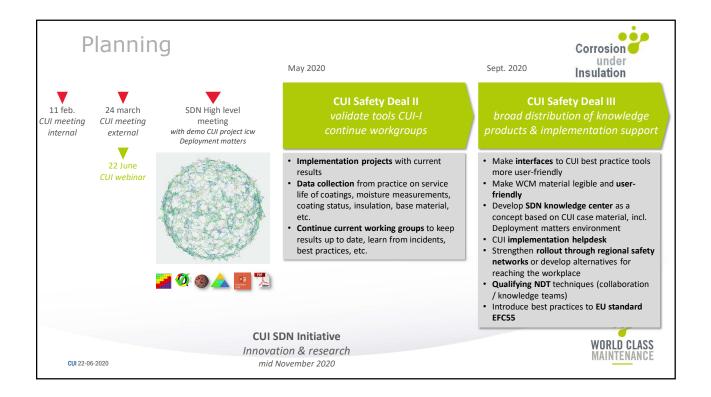






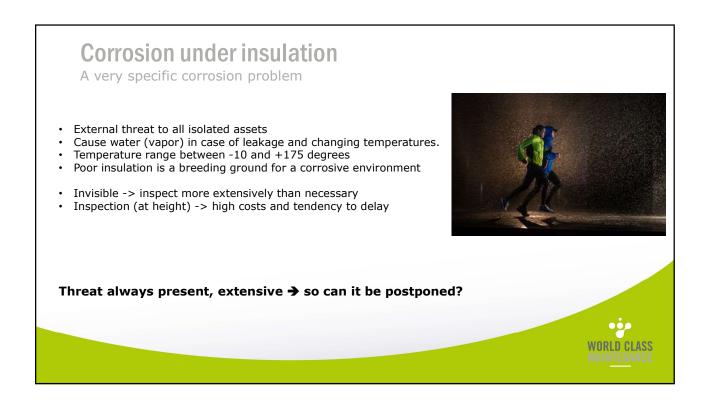




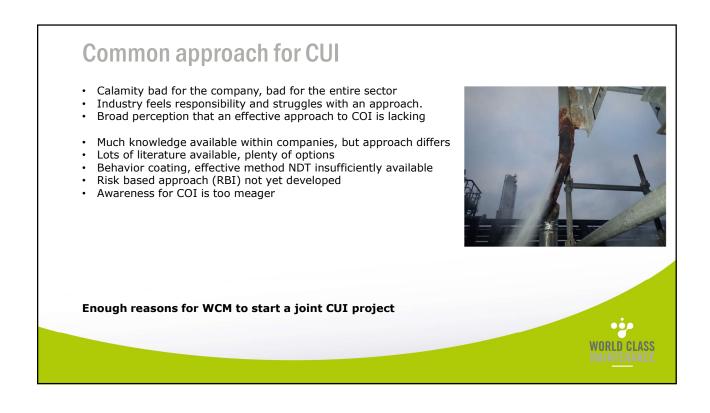


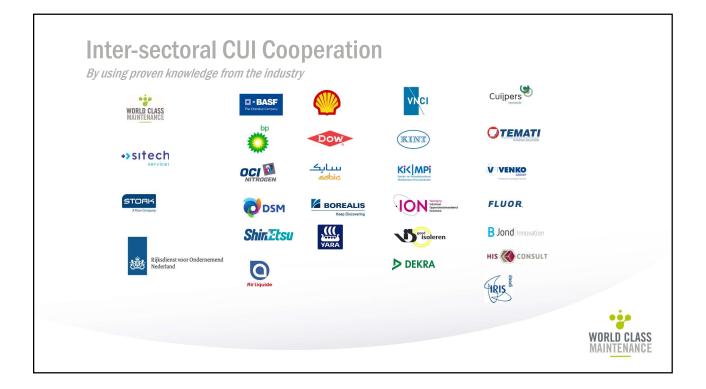




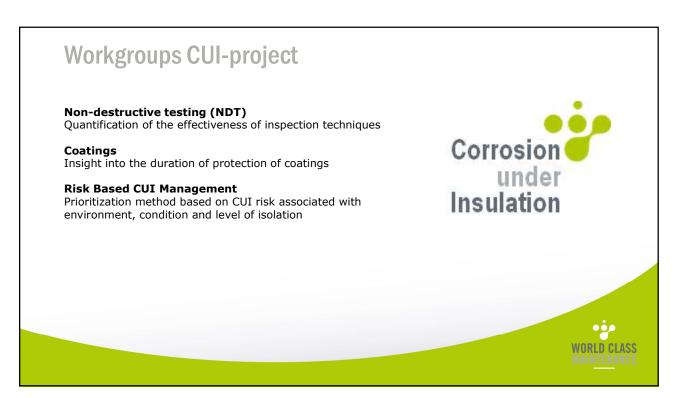


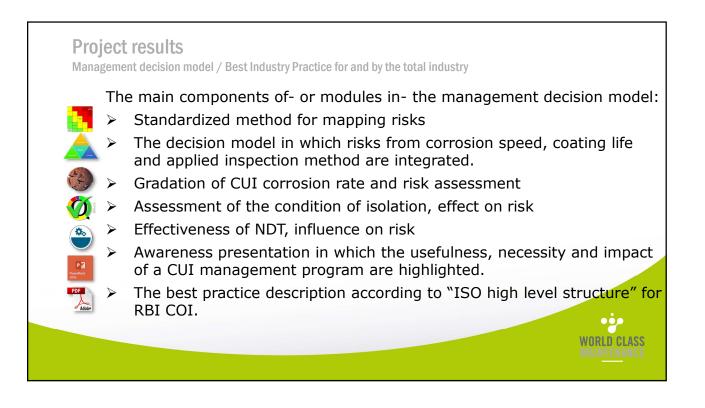


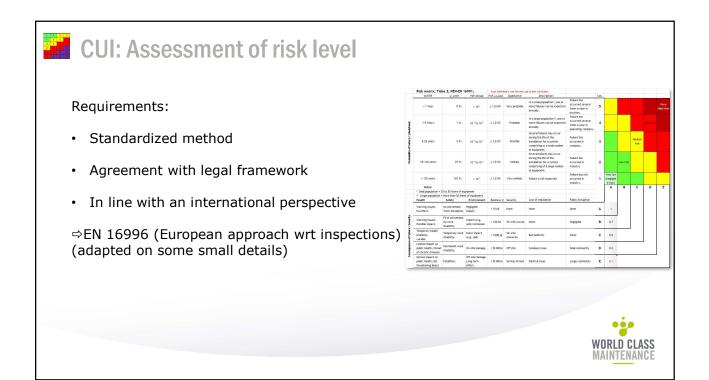


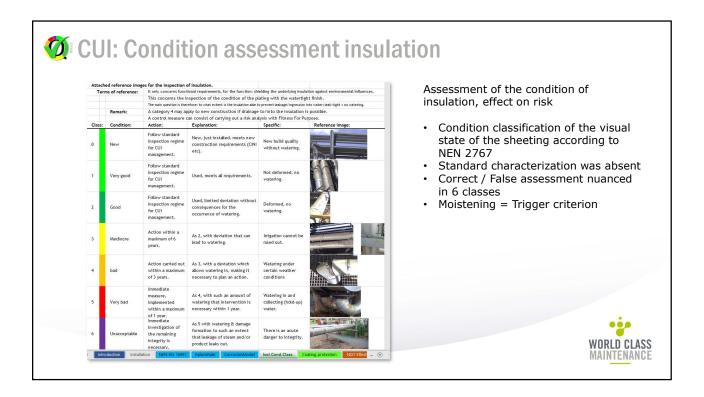


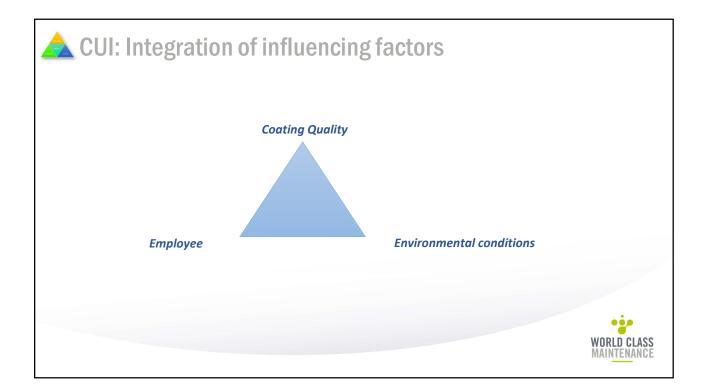


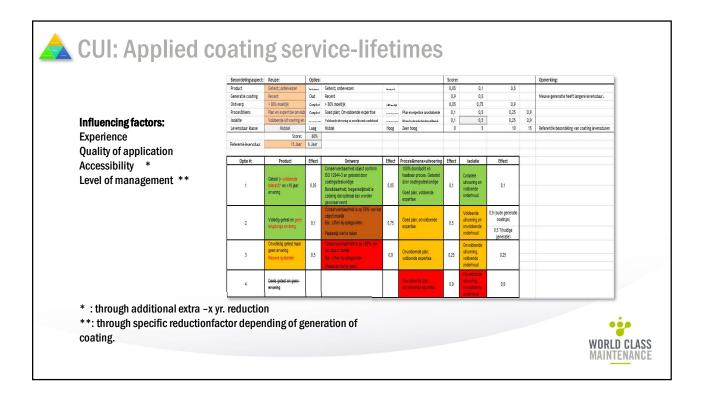


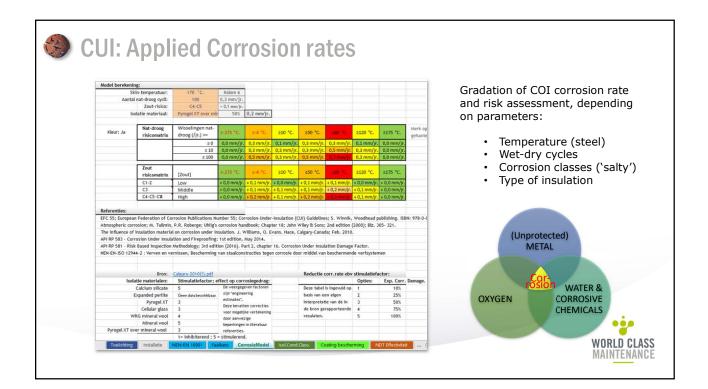


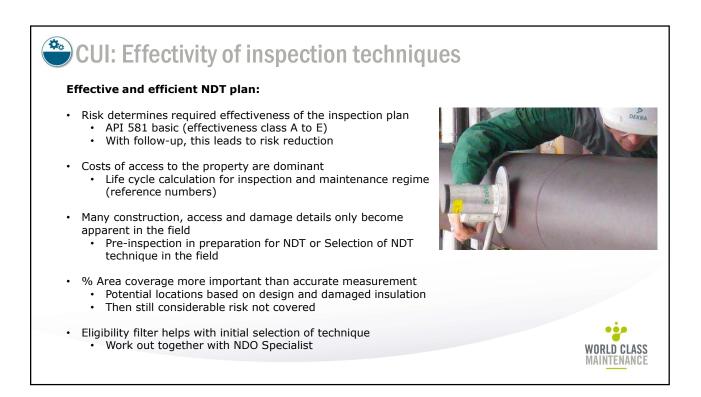












Geschiktheidsfilter NDO technieken	Corrosie onder Isolatie		Required effectiveness
Object type	Aftakkingen op leidingen > DN250 en op vatwanden		 Leads to required coverage
Beoogd doel	Corrosie detectie		1 5
Vereiste inspectie-effectiviteit	B= Usually Effective		
Vereiste dekking	65%		Intended purpose
Diameter (mm)	250		
Nom. Wanddikte (mm)	.6		 Moisture, corrosion, wall thickne
Toegankelijkheid	Vanaf grond of bordes toegankelijk		
	Vanaf grond of bordes toegankelijk Vanaf steiger werken Hoogverker, rope access Ondergronds		Object type and geometry
Geschikte NDO technieken	Opmerkingen		 Pipeline, vessel, branches, …
On stream RT (film)	Beperkt toepasbaar voor wanddiktemeting (HOIS Recommended Practice 1 v3.1)		 Nominal wall thickness
On stream RT (digitaal)	Beperkt toepasbaar voor wanddiktemeting (HOIS Recommended Practice 1 v3.1)		Norminal Wall Chickless
Profile radiografie	Beperkt toepasbaar voor vochtdetectie (HOIS Recomm	ended Practice 1 v3.1)	
In-line inspection (intelligent pigging)			Accessibility
Visuele inspectie met uitpakken			First estimate what should be applied

